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Nonlinear Control Design and Analysis of a Multi-Terminal VSC-HVDC System

Yijing Chen¹, Jing Dai¹, Gilney Damm², Françoise Lamnabhi-Lagarrigue¹

Abstract—This paper presents a nonlinear control strategy based on dynamic feedback linearization control theory and a backstepping-like procedure for a multi-terminal voltage-source converter based high-voltage direct current (multi-terminal VSC-HVDC) system. The controller is able to provide global asymptotic stability for the power transmission system consisting of N terminals. Furthermore it is shown that the remaining zero dynamics (mostly representing the DC network) are also exponentially stable, and then the whole system can be shown asymptotically stable. These results are obtained by a rigorous stability proof for the whole system under the proposed controller, and its performance is illustrated by computer simulations.

I. INTRODUCTION

With the development of wind, solar and other renewable energy sources, there is an urgent need to integrate these decentralized and relatively small-scale power plants into the grid in an economical and environmentally friendly way. Furthermore, the increase of electricity demand requires the expansion of grid capacity. But it is very hard to increase the grid through overhead AC lines, which occupy large transmission line corridors. For both cases, Voltage-Source Converter based High-Voltage Direct Current (VSC-HVDC) multipoint networks could be a good solution.

At present, over 90 DC transmission projects exist in the world, the vast majority for point-to-point two-terminal HVDC transmission system and only two for multi-terminal HVDC (MTDC) system. The traditional two-terminal HVDC transmission system can only carry out point-to-point power transfer. Under the requirements of the economic development and the construction of the power grid, it is necessary to require that the DC grid can achieve power exchanges among multiple power suppliers and multiple power consumers. Therefore, the MTDC system based on the two-terminal HVDC system draws more and more attention. MTDC transmission system is a DC transmission network connecting more than two converter stations (AC/DC, DC/DC). It offers a large transmission capacity (larger than the AC network) and can provide a more flexible, efficient transmission way. The main applications of MTDC system include the power exchange among multi-points, integrating isolated asynchronous networks, and integrating scattered power plants like offshore renewable energy sources such as wind, hydro, solar.

On the other hand, MTDC system brings several stability problems. The strong interaction between DC and AC networks may lead to a significant decrease in the overall system performance and even threaten the stability and safety of the system. Therefore, it is important to perform a rigorous mathematical stability analysis for the MTDC system.

A large amount of research on two-terminal VSC HVDC control has been carried out [1], [2], [3], [4]. In [1], an equivalent continuous-time averaged state-space model is presented and a robust DC-bus voltage control scheme is proposed highlighting the existence of fast and slow dynamics that can be associated to the inner current control loop and outer DC-bus voltage control loop. Reference [3] proposes a control strategy under balanced and unbalanced network conditions, which contains two sets of controller: a main controller in the positive dq frame using decoupling control, and an auxiliary controller using coupling control. However, the above mentioned controllers were designed for a standard two-terminal VSC-HVDC system, not for multi-terminal VSC-HVDC system. In [5], [6], [7], control strategies of VSC based multi-terminal were investigated. Reference [7] uses a droop control scheme to control the DC voltage. Reference [5] presents a multi-point DC voltage control and [6] proposes a scheme for controlling and coordinating the grid. However, the previously mentioned articles came from the power systems' community, and as a consequence, did not provide stability proofs.

In the present paper, a control strategy is formally designed with its mathematical stability analysis for a multi-terminal HVDC system. The controller is developed following a dynamic feedback linearization strategy that, by a naturally decoupled time-scale phenomenon, represents a backstepping-like control strategy (see [8][9][10]). This controller assures global asymptotic stability for the power transmission system consisting of N terminals. In a second step, the behavior of the remaining states of the system (known as the zero dynamics) is analyzed, which is given by the transmission network. And the zero dynamics are shown to be exponentially stable. It can then be seen that the whole MTDC system is asymptotically stable. This paper is organized into five sections. In Section II, a dynamic multi-terminal VSC HVDC model is given. In Section III, a feedback control law is developed. Simulations are carried out in Section IV. Conclusions are drawn in Section V.

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II. MODELING OF A MULTI-TERMINAL VSC-HVDC SYSTEM

This section introduces the state-space model of a multi-terminal VSC-HVDC system established in the synchronous dq frame, which allows for a decoupled control on the active and the reactive power, where the high-frequency PWM characteristics of the power electronics are neglected. Only the balanced condition is considered in this paper, i.e. the three phases have identical parameters and their voltages and currents have the same amplitude while phase-shifted 120° between themselves.

A converter of a multi-terminal VSC HVDC system connected to other converters is shown in Fig. 1.

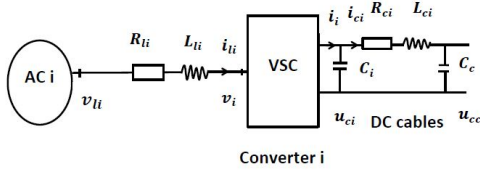


Fig. 1. One terminal in a multi-terminal VSC Transmission System

AC network

On the AC side of the converter station, the Kirchhoff voltage law leads to the system expressed in dq synchronous reference frame rotating at the pulsation ω_i :

$$v_{lid} - R_{li}\dot{i}_{lid} - L_{li}\frac{d\dot{i}_{lid}}{dt} + \omega_i L_{li}\dot{i}_{liq} - v_{id} = 0 \quad (1a)$$

$$v_{liq} - R_{li}\dot{i}_{liq} - L_{li}\frac{d\dot{i}_{liq}}{dt} - \omega_i L_{li}\dot{i}_{lid} - v_{iq} = 0 \quad (1b)$$

By using Pulse Width Modulation (PWM) technology, the amplitude of the converter output voltage v_{id} and v_{iq} are controlled by the modulation index as:

$$v_{id} = \frac{v_{idw}}{2}u_{ci} \quad (2a)$$

$$v_{iq} = \frac{v_{iqw}}{2}u_{ci} \quad (2b)$$

By neglecting the resistance of the converter reactor and switching losses, the instantaneous active power and reactive power on the AC side of the converters can be expressed as follows:

$$P_{li} = \frac{3}{2}(v_{lid}\dot{i}_{lid} + v_{liq}\dot{i}_{liq}) \quad (3)$$

$$Q_{li} = \frac{3}{2}(v_{liq}\dot{i}_{lid} - v_{lid}\dot{i}_{liq}) \quad (4)$$

DC line

By applying the Kirchhoff voltage and current laws to the DC circuit, the DC side of the rectifier is modelled by the following differential equations:

$$\frac{du_{ci}}{dt} = -\frac{1}{C_i}i_{ci} + \frac{1}{C_i}i_i \quad (5)$$

$$\frac{di_{ci}}{dt} = \frac{1}{L_{ci}}u_{ci} - \frac{R_{ci}}{L_{ci}}i_{ci} - \frac{1}{L_{ci}}u_{cc} \quad (6)$$

AC-DC power coupling

Considering the active power balance on both sides of the converter, we have $u_{ci}i_i = v_{iA}\dot{i}_{liA} + v_{iB}\dot{i}_{liB} + v_{iC}\dot{i}_{liC}$. Thus, i_i can be expressed as the following equations:

$$i_i = \frac{3}{4}(v_{idw}\dot{i}_{lid} + v_{iqw}\dot{i}_{liq}) \quad (7)$$

The interconnection among N terminals, as shown in Fig. 2, is represented as follows:

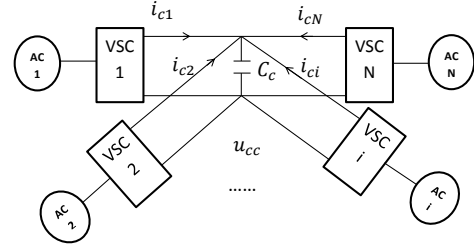


Fig. 2. The interconnection of a multi-terminal VSC Transmission System

$$\frac{du_{cc}}{dt} = \frac{1}{C_c} \sum_{i=1}^N i_{ci} \quad (8)$$

Global model

The full state-space model of N -terminal VSC-HVDC system is written as follows:

$$\begin{cases} \dot{i}_{lid} = -\frac{R_{li}}{L_{li}}i_{lid} + \omega_i i_{liq} - \frac{1}{L_{li}}v_{idw}\frac{u_{ci}}{2} + \frac{1}{L_{li}}v_{lid} \\ \dot{i}_{liq} = -\frac{R_{li}}{L_{li}}i_{liq} - \omega_i i_{lid} - \frac{1}{L_{li}}v_{iqw}\frac{u_{ci}}{2} + \frac{1}{L_{li}}v_{liq} \\ \dot{u}_{ci} = -\frac{1}{C_i}i_{ci} + \frac{1}{C_i}\frac{3}{4}(v_{idw}\dot{i}_{lid} + v_{iqw}\dot{i}_{liq}) \\ \dot{i}_{ci} = \frac{1}{L_{ci}}u_{ci} - \frac{R_{ci}}{L_{ci}}i_{ci} - \frac{1}{L_{ci}}u_{cc} \\ \dot{u}_{cc} = \frac{1}{C_c}(\sum_{i=1}^N i_{ci}) \end{cases} \quad (9)$$

where $i = 1, \dots, N$.

The global state-space model of the multi-terminal VSC-HVDC system is summarized as follows:

- State variables: $i_{lid}, i_{liq}, u_{ci}, \dot{i}_{ci}, u_{cc}$.
- Control variables: v_{idw}, v_{iqw} .
- External parameters: v_{lid}, v_{liq} .
- External references provided by a higher level controller named the HVDC secondary controller: u_{ci}^*, Q_{li}^* .
- The dimension of the system (9) is $4N + 1$.

III. CONTROL SCHEME

In this part we will present the detailed synthesis of the controller for one of the terminals, i.e. addressing the converter's DC voltage u_{ci} and reactive power Q_{li} .

For the converter modelled by the first three equations of the system (9), it is desired that the dq currents i_{lid}, i_{liq} and the DC voltage u_{ci} track their reference values.

The control structure is mainly based on the following physical considerations:

- The dynamics of the original system expressed by (9) highlights a separation into fast and slow dynamics, where the DC voltage equation represents the slow dynamics, and the dq current equations represent the fast dynamics. Thus, this multitime-scale behaviour suggests to apply a cascaded control system. The inner control loop will control the fast dynamics i_{lid} and i_{liq} and the outer control loop will regulate the slow dynamics u_{ci} and control reactive power Q_i . The outputs of the outer control loop provides the current reference points in the dq frame i_{lid}^* and i_{liq}^* for the inner loop system.
- We consider dq frame right orientation such that $v_{liq} = 0$, then (4) can be written as, $Q_{li} = -\frac{3}{2}v_{lid}i_{liq}$, which means that the reactive power is directly controlled i_{liq} .

A backstepping-like procedure is carried out for designing the control scheme. In the first step, the backstepping-like procedure requires the fast dynamics AC currents i_{lid} and i_{liq} to follow their reference trajectories (yet to be designed), which means to eliminate the dq current errors \tilde{i}_{lid} and \tilde{i}_{liq} where $\tilde{i}_{lid} = i_{lid} - i_{lid}^*$, $\tilde{i}_{liq} = i_{liq} - i_{liq}^*$.

Following a feedback linearization objective, we design the control laws:

$$u_{id} = \dot{i}_{lid} \triangleq \dot{\tilde{i}}_{lid} + \dot{i}_{lid}^* \quad (10a)$$

$$u_{iq} = \dot{i}_{liq} \triangleq \dot{\tilde{i}}_{liq} + \dot{i}_{liq}^* \quad (10b)$$

The currents i_{lid} and i_{liq} are controlled independently by the auxiliary inputs u_{id} and u_{iq} obtaining the new systems as follows:

$$v_{idw} = \frac{2L_{li}}{u_{ci}} \left(-\frac{R_{li}}{L_{li}} \dot{i}_{lid} + \omega_i i_{liq} + \frac{1}{L_{li}} v_{lid} - u_{id} \right) \quad (11a)$$

$$v_{iqw} = \frac{2L_{li}}{u_{ci}} \left(-\frac{R_{li}}{L_{li}} \dot{i}_{liq} - \omega_i i_{lid} + \frac{1}{L_{li}} v_{liq} - u_{iq} \right) \quad (11b)$$

To assure that the errors \tilde{i}_{lid} and \tilde{i}_{liq} will converge to zero, as well as good steady states, it is proposed the following augmented state:

$$\dot{\varphi}_{id} = \tilde{i}_{lid} \quad (12a)$$

$$\dot{\tilde{i}}_{lid} = -k_{id}\tilde{i}_{lid} - \lambda_{id}\varphi_{id} \quad (12b)$$

and

$$\dot{\varphi}_{iq} = \tilde{i}_{liq} \quad (13a)$$

$$\dot{\tilde{i}}_{liq} = -k_{iq}\tilde{i}_{liq} - \lambda_{iq}\varphi_{iq} \quad (13b)$$

where k_{id} , k_{iq} , λ_{id} and λ_{iq} are positive constants. Thus, we have:

$$u_{id} = -k_{id}\tilde{i}_{lid} - \lambda_{id}\varphi_{id} + \dot{i}_{lid}^* \quad (14a)$$

$$u_{iq} = -k_{iq}\tilde{i}_{liq} - \lambda_{iq}\varphi_{iq} + \dot{i}_{liq}^* \quad (14b)$$

The second step of the backstepping-like procedure determines the behaviour of the converter, which include DC voltage control and reactive power control. The outputs of

this step provide the dq current reference values for dq currents.

The trajectory i_{liq}^* is obtained directly from the reactive power's reference provided by the secondary level (possibly from the AC voltage controller):

$$i_{liq}^* = -\frac{2}{3} \frac{Q_{li}^*}{v_{lid}} \quad (15)$$

One of the goals of the proposed controller is to keep the DC voltage constant at its reference point u_{ci}^* . It is this DC voltage controller that provides i_{liq}^* to the inner controllers.

Placing (11) into the third equation of (9), we have:

$$\begin{aligned} \dot{u}_{ci} = & -\frac{1}{C_i} i_{ci} + \frac{3}{2} \frac{1}{C_i u_{ci}} [i_{lid}(-R_{li}i_{lid} + v_{lid} - L_{li}u_{id}) \\ & + i_{liq}(-R_{li}i_{liq} + v_{liq} - L_{li}u_{iq})] \end{aligned} \quad (16)$$

Then, by substituting (11) into (16), the DC voltage dynamics is given by:

$$\begin{aligned} \dot{u}_{ci} = & -\frac{1}{C_i} i_{ci} + \frac{3}{2} \frac{1}{C_i u_{ci}} \cdot \\ & [i_{lid}(-R_{li}i_{lid} + v_{lid} + L_{li}k_{id}\tilde{i}_{lid} + L_{li}\lambda_{id}\varphi_{id} - L_{li}\dot{i}_{lid}^*) \\ & + i_{liq}(-R_{li}i_{liq} + v_{liq} + L_{li}k_{iq}\tilde{i}_{liq} + L_{li}\lambda_{iq}\varphi_{iq} - L_{li}\dot{i}_{liq}^*)] \end{aligned} \quad (17)$$

Since it is aimed to maintain the DC voltage u_{ci} at its set value, the desired dynamics of voltage error \tilde{u}_{ci} is expressed as:

$$\dot{\varphi}_{ci} = \tilde{u}_{ci} \quad (18a)$$

$$\dot{\tilde{u}}_{ci} = -k_{ci}\tilde{u}_{ci} - \lambda_{ci}\varphi_{ci} \quad (18b)$$

where $\tilde{u}_{ci} = u_{ci} - u_{ci}^*$. The above equation can also be written as:

$$\dot{u}_{ci} = -k_{ci}\tilde{u}_{ci} - \lambda_{ci}\varphi_{ci} + \dot{u}_{ci}^* \quad (19)$$

Since the desired values for u_{ci}^* , Q_{li}^* are constant, \dot{u}_{ci}^* and \dot{i}_{liq}^* are taken as zero.

It is then clear that to transform the actual dynamics (17) into the desired (18b), it's necessary to apply the control:

$$\begin{aligned} i_{lid}^* = & -\frac{2}{3} \frac{u_{ci}}{i_{lid}} \frac{C_i}{L_{li}} (-k_{ci}\tilde{u}_{ci} - \lambda_{ci}\varphi_{ci} + \frac{\dot{u}_{ci}}{C_i}) + \frac{u_{ci}}{2L_{li}} \frac{\dot{i}_{liq}}{i_{lid}} v_{iqw} \\ & + (-\frac{R_{li}}{L_{li}} \dot{i}_{lid} + \omega_i i_{liq} + \frac{v_{lid}}{L_{li}} + k_{id}\tilde{i}_{lid} + \lambda_{id}\varphi_{id}) \end{aligned} \quad (20)$$

The main result of this paper can be then summarized in the form of the theorem:

Theorem 1: The multi-terminal VSC-HVDC system described by (9) under the control laws (11)-(20) is globally asymptotically stabilized to the actual reference values u_{ci}^* and Q_{li}^* . Furthermore, this result is independent of the network's parameters L_{ci} , R_{ci} , C_{ci} .

Proof: In the considered case, the N converters drive the DC voltage. It is desired to keep u_{ci} and Q_{li} at their reference values u_{ci}^* and Q_{li}^* . Thus the outputs of the system can be defined as:

$$y = [u_{ci} \ Q_{li}]^T \quad (21)$$

From the previous section, we know that i_{lid}^* , i_{liq}^* are defined by (15) and (20).

To simplify our problem, at first, we shift the reference values of the whole system to the origins and the following new state variables are introduced:

$$\tilde{x} = [\tilde{i}_{lid} \tilde{i}_{liq} \tilde{u}_{ci} \tilde{i}_{ci} \tilde{u}_{cc}]^T \quad (22)$$

where $\tilde{i}_{ci} = i_{ci} - i_{ci}^*$, $\tilde{u}_{cc} = u_{cc} - u_{cc}^*$ with i_{ci}^* and u_{cc}^* the equilibrium values of i_{ci} and u_{cc} .

And the new output error variables as follows:

$$\tilde{y} = [\tilde{u}_{ci} \tilde{Q}_{li}]^T \quad (23)$$

where $\tilde{Q}_{li} = Q_{li} - Q_{li}^*$.

The system (9) can be expressed in the new error variables as:

$$\begin{cases} \frac{d\tilde{i}_{lid}}{dt} = -\frac{R_{li}\tilde{i}_{lid}}{L_{li}} + \omega_i \tilde{i}_{liq} - \frac{1}{L_{li}} v_{idw} \frac{\tilde{u}_{ci}}{2} \\ \frac{d\tilde{i}_{liq}}{dt} = -\frac{R_{li}\tilde{i}_{liq}}{L_{li}} - \omega_i \tilde{i}_{lid} - \frac{1}{L_{li}} v_{iqw} \frac{\tilde{u}_{ci}}{2} \\ \frac{d\tilde{u}_{ci}}{dt} = -\frac{1}{C_i} \tilde{i}_{ci} + \frac{1}{C_i} \frac{3}{4} (v_{idw} \tilde{i}_{lid} + v_{iqw} \tilde{i}_{liq}) \\ \frac{d\tilde{i}_{ci}}{dt} = \frac{1}{L_{ci}} \tilde{u}_{ci} - \frac{R_{ci}\tilde{i}_{ci}}{L_{ci}} - \frac{1}{L_{ci}} \tilde{u}_{cc} \\ \frac{d\tilde{u}_{cc}}{dt} = \frac{1}{C_c} (\sum_{i=1}^N \tilde{i}_{ci}) \end{cases} \quad (24)$$

where $i = 1, \dots, N$.

Now in order to analyze the stability of the new system (24), we first divide the state variables \tilde{x} into two parts:

$$\eta = [\tilde{i}_{ci} \tilde{u}_{cc}]^T, \quad (25a)$$

$$\xi = [\tilde{i}_{lid} \tilde{i}_{liq} \tilde{u}_{ci}]^T. \quad (25b)$$

The system (24) can be considered as in the normal form:

$$\dot{\eta} = f_1(\eta, \xi), \quad (26a)$$

$$\dot{\xi} = f_2(\eta, \xi, u). \quad (26b)$$

with

$$u = f_3(\eta, \xi). \quad (27)$$

This is the standard nonlinear zero dynamics form [9]. If a system is in the normal form (26), when ξ is identically zero, the behaviour of the system (26) is governed by the differential equation:

$$\dot{\eta} = f_1(\eta, 0) \quad (28)$$

The dynamics of (28) correspond to the "internal" behaviour of the system, which are called the zero dynamics of the system. Suppose that $\eta = 0$ of the zero dynamics of the system (26) is globally asymptotically stable and ξ is also globally asymptotically stable under the feedback control law (27), then the whole system (26) is stabilized by the feedback control law (27) at $(\eta, \xi) = (0, 0)$ [9].

The next step is to study the behaviours of η, ξ respectively. Applying the controller (11) and (12) (13) (18), the closed-loop error system can be written as:

$$\dot{\zeta} = A\zeta \quad (29)$$

where $\zeta = [\varphi_{id} \tilde{i}_{lid} \varphi_{iq} \tilde{i}_{liq} \varphi_{ci} \tilde{u}_{ci}]^T$ and $A = \text{diag}(A_{id}, A_{iq}, A_{ci})$ with

$$\begin{aligned} A_{id} &= \begin{pmatrix} 0 & 1 \\ -\lambda_{id} & -k_{id} \end{pmatrix} \\ A_{iq} &= \begin{pmatrix} 0 & 1 \\ -\lambda_{iq} & -k_{iq} \end{pmatrix} \\ A_{ci} &= \begin{pmatrix} 0 & 1 \\ -\lambda_{ci} & -k_{ci} \end{pmatrix} \end{aligned} \quad (30)$$

It is easy to verify that matrix A is Hurwitz. Thus, ζ is globally exponentially stable with the proposed control law (11). It is now necessary to study the behaviour of the state variables η when ξ converge to zero. In fact, when $\xi = 0$, η is governed by the following differential equation:

$$\begin{bmatrix} \dot{\tilde{i}_{c1}} \\ \dot{\tilde{i}_{c2}} \\ \vdots \\ \dot{\tilde{i}_{cN}} \\ \dot{\tilde{u}_{cc}} \end{bmatrix} = \begin{bmatrix} -\frac{R_{c1}}{L_{c1}} & 0 & \dots & 0 & -\frac{1}{L_{c1}} \\ 0 & -\frac{R_{c2}}{L_{c2}} & \dots & 0 & -\frac{1}{L_{c2}} \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & 0 & \dots & -\frac{R_{cN}}{L_{cN}} & -\frac{1}{L_{cN}} \\ \frac{1}{C_c} & -\frac{1}{C_c} & \dots & -\frac{1}{C_c} & 0 \end{bmatrix} \begin{bmatrix} \tilde{i}_{c1} \\ \tilde{i}_{c2} \\ \vdots \\ \tilde{i}_{cN} \\ \tilde{u}_{cc} \end{bmatrix} \quad (31)$$

Thus, the zero dynamics of the system (24) is:

$$f_1(\eta, 0) = B\eta \quad (32)$$

$$\text{where } B = \begin{bmatrix} -\frac{R_{c1}}{L_{c1}} & 0 & \dots & 0 & -\frac{1}{L_{c1}} \\ 0 & -\frac{R_{c2}}{L_{c2}} & \dots & 0 & -\frac{1}{L_{c2}} \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ \frac{1}{C_c} & -\frac{1}{C_c} & \dots & -\frac{1}{C_c} & 0 \end{bmatrix}.$$

The characteristic polynomial of matrix B is in the following form:

$$f(\lambda) = \lambda^{N+1} + \sum_{i=0}^N a_i \lambda^i \quad (33)$$

where λ are the eigenvalues of matrix B and $a_i, i = 0, \dots, N$ are positive.

For all λ , $Re(\lambda)$ is negative and as consequence, B is Hurwitz and then the zero dynamics of the system (24) $\dot{\eta} = f_1(\eta, 0)$ is globally exponentially stable. ■

From the above proof, the designed control law (11) can globally exponentially stabilize ξ and the zero dynamics (28) is also globally exponentially stable. Finally the whole system (24) is globally asymptotically stabilized at $(\eta, \xi) = (0, 0)$ by the proposed controller.

IV. SIMULATION RESULTS

The proposed controller is tested in computer simulations presenting a three-terminal VSC-HVDC system, which is shown in Fig. 3. These three VSC terminal operate in DC voltage control mode. The parameter values are presented in Table I. We choose the pulsation $\omega_i = 314$, the capacitor $C_i = 12 \times 10^{-6}$ F and the RMS value of $v_{li} = 230 \times 10^3$ V.

TABLE I
PARAMETER VALUES OF EACH AC AREA.

	R_{li}	L_{li}	R_{ci}	L_{ci}
AC 1	13.79	31.02e-3	0.2085	0.0024
AC 2	12.79	33.02e-3	0.2	0.001
AC 3	13.57	40.02e-3	0.235	0.0035

TABLE II
SEQUENCE OF EVENTS ASSUMED IN SIMULATION

Time (s)	Events
0	Initial settings: $u_{c1} = 101$ KV, $u_{c2} = 100$ KV, $u_{c3} = 99.8$ KV
1	Set the reference values: $u_{c1} = 101.2$ KV, $u_{c2} = 101$ KV, $u_{c3} = 99.9$ KV
4	Set the reference value: $u_{c1} = 102.2$ KV
5	Set the reference value: $u_{c2} = 102.0$ KV
6	Set the reference value: $u_{c3} = 100.9$ KV

The feedback control gains are given as $k_{id} = 100$, $\lambda_{id} = 100$, $k_{iq} = 100$, $\lambda_{iq} = 100$, $k_{ci} = 25$, $\lambda_{ci} = 5$. The sequence of values listed in Table II is used when carrying out the simulations. And In our simulations, all reactive powers Q_{l1} , Q_{l2} and Q_{l3} are set up to zero which allow unitary power factor, which means that i_{l2q}^* , i_{l2q}^* and i_{l3q}^* are zero.

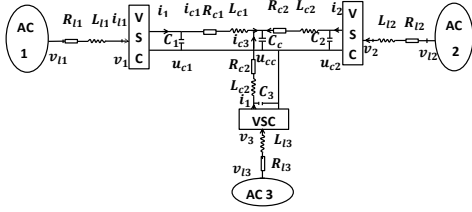


Fig. 3. A three-terminal VSC-HVDC Transmission System

Simulation results are shown in Fig. (4)-(9). The regulation behaviours of each converter's DC voltage are illustrated in Fig. (4), (5) and (6) where the black curve represents each DC voltage's reference value and the red one is its responses. At the start of the simulation, these terminals work at their initial reference values, then at $t = 1s$, there are a step change for each DC voltage reference values. Fig. (4)-(6) indicate that each DC voltage u_{ci} reaches its new reference value before $t = 2s$. At $t = 4s$, we only give a step change for u_{c1}^* , after then u_{c1} achieve its new reference value before $t = 5$ as can be seen in Fig. (4). During $t = 4s$ to $t = 5s$, u_{c2} and u_{c3} keep unchanging and are still at their own reference values as shown in Fig. (5) and (6). At $t = 5s$ and $t = 6s$, when the reference values for u_{c2} and u_{c3} are reset, respectively, we find that, they attain their new references and have no effect to u_{c1} .

The converter's quadrature current i_{liq} are always very close to zero no matter how the DC voltage reference value change. The reason is that the quadrature current is controlled by the reactive controller. If the reference value of Q_{li} is always zero, i_{liq} remains close to zero.

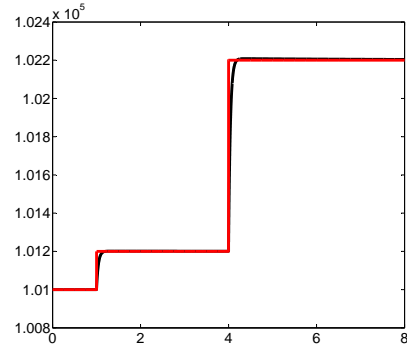


Fig. 4. DC voltage control u_{c1} reference and response

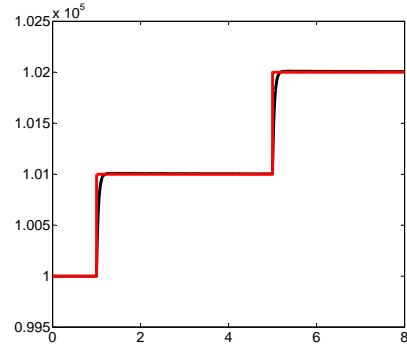


Fig. 5. DC voltage control u_{c2} reference and response

Fig. (7), (8) and (9) illustrate each converter's direct current i_{lid} . We can see that, once the DC voltage reference value change, the direct current also change and reach a new reference point. It is true since i_{lid}^* is controlled by DC voltage controller.

V. CONCLUSIONS

In this paper, a nonlinear controller has been designed for the multi-terminal VSC-HVDC system. This controller is a cascade control system that exhibits a multitime-scale behaviour. The proposed control law is based on dynamic feedback linearization strategy and a backstepping-like procedure. A detailed stability analysis by means of the zero dynamics approach for the nonlinear system shows that the MTDC system is asymptotically stable. Simulation results also clearly show that the proposed control strategy contributes significantly to regulating DC-bus voltage and it highlights dynamic performances.

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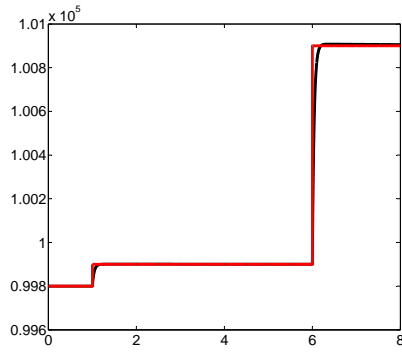


Fig. 6. DC voltage control u_{c3} reference and response

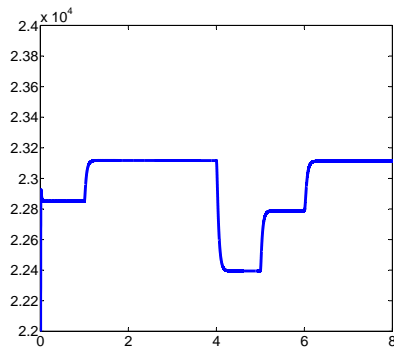


Fig. 7. DC voltage control i_{l1d} response

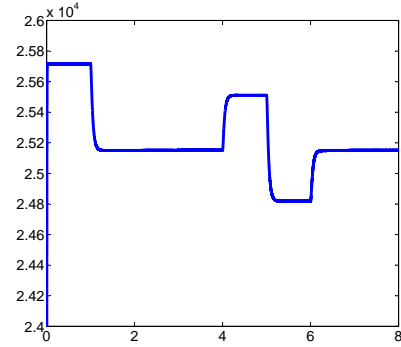


Fig. 8. DC voltage control i_{l2d} response

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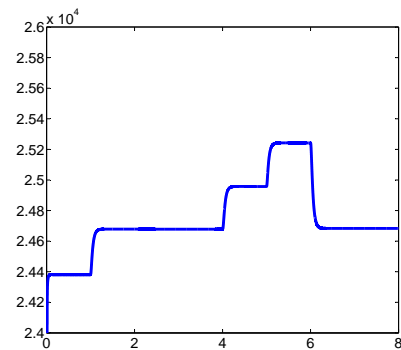


Fig. 9. DC voltage control i_{l3d} response