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Etienne Servais, Brigitte d'Andréa-Novel, Hugues Mounier. Motion Planning for Multi-Agent Systems Using Gevrey Trajectories Based on Burgers' Viscous Equation. 19th IFAC World Congress on International Federation of Automatic Control (IFAC 2014), IFAC, Aug 2014, Cape Town, South Africa. ⟨hal-01100841⟩

**HAL Id: hal-01100841**

**<https://centralesupelec.hal.science/hal-01100841v1>**

Submitted on 7 Jan 2015

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# Motion Planning for Multi-Agent Systems Using Gevrey Trajectories Based on Burgers' Viscous Equation <sup>\*</sup>

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**Abstract:** The differential flatness of the one-dimensional heat equation controlled at each boundary is used to propose, through the Hopf-Cole transform, a finite-time motion planning for multi-agent systems. The proposed paths, which are solutions of Burgers' viscous equation, are smooth while non analytical in initial and final equilibria. The paths may respect various geometrical constraints allowing them to be used for different purposes.

*Keywords:* Nonlinear partial differential equations, flatness, multi-agent systems, autonomous mobile robots, robot navigation, trajectory planning

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## 1. INTRODUCTION

Since the introduction of computer animations back in the late 80' and the need of reliably animate swarm of birds, herds and flocks (see Reynolds (1987)), several ways of animating and moving multi-agent systems have been proposed. In the past years, this field has been thoroughly studied due to the appearance of new multi-agent systems: unmanned autonomous vehicles (so called *UAV*'s) such as quadrotors and mobile robots.

The different methods can be either distributed or centralized depending on the knowledge of a single agent of the state of the global system. Systems needing informations about the states of all the agents are called to be centralized whereas systems where agents can be moved knowing only informations on their nearest neighbors are called decentralized. The main goal of the techniques are collision avoidance (with other agents or obstacles), cohesion of the system and the final stabilization on a specific formation or trajectory.

Various methods either distributed or centralized have been proposed using potential-like solutions (Olfati-Saber and Murray (2002)), geometric approaches (Briñon Arranz et al. (2011)) or based on graph theory (see Ferrari-Trecate et al. (2006); Fax and Murray (2002)) and receding horizons methods (Murray and Dunbar (2004)).

Our method, based on previous works by Frihauf and Krstic (2011); Meurer and Krstić (2011) considers the multi-agent system as a continuum of fully actuated agents and steers it using Partial Differential Equations (**PDE**'s). It accomplishes full stabilization of the system and collision avoidance using the physical model described by

the chosen PDE. The problem of PDE control is a wide open subject and only few problems are yet solved, using for example either *differential flatness* (see Laroche et al. (2000); Meurer and Krstić (2011)) or the newly introduced *backstepping* method by Krstić and Smyshlyaev (2008).

In this paper, we use the *Hopf-Cole* transformation by Hopf (1950) and Cole et al. (1951) to transform the viscous Burgers' equation  $u_t + uu_x = \mu u_{xx}$  into the heat equation, which was already proven to be in some case differentially flat (see for instance Laroche et al. (2000)).

The controllability of Burgers' viscous equation with two boundary controls has been recently broadly studied and various results have been obtained. On the one hand Guerrero and Imanuvilov (2007) proved that both the global exact null controllability for small time and the exact controllability for large time do not hold. On the other hand, Glass and Guerrero (2007) gives a proof of the global exact null controllability to nonzero states and Coron (2007) has shown using the Hopf-Cole transformation a controllability result to large constant states.

In our case we use two inputs on either side of the system. These inputs describe the trajectories of two leaders of the formation. We use the Hopf-Cole transformation in section 2 and prove some flatness properties of the heat equation. We then propose in section 3 a Gevrey (1918) solution respecting initial and final formations constraints both in the real space (in which we solve Burgers' equation) and in the Hopf-Cole space (in which we solve the heat equation). When using only the heat equation, trajectory checkpoints might be used by the two boundary agents. We evaluate our controls through numerical computations and propose a formal expression of the solution. We then test our controls for the heat equation against formal solution and constraints. Some examples for the motion planning based on the Hopf-Cole equation are finally given.

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<sup>\*</sup> This work was supported by DIGITEO grant 2011-043D and by the Région Île-de-France

## 2. FLATNESS PROPERTIES

The steering of PDE's is a problem widely studied in industry. It allows motion planning, *i.e.* the ability to move a system such as a chemical reactor in Fliess et al. (1998) or a crystal in Rudolph et al. (2004) from a known state to another state on a determined path. Burgers' equation is a standard PDE of the fluid mechanics. It is sometimes thought as the 1D analogue of Navier-Stokes 2D equations. As one of the simplest non-linear PDE, it is a common choice allowing shock-like equilibria (see Krstić et al. (2008)) and has been used for motion-planning tasks (see Krstić et al. (2009); Meurer and Krstić (2011)).

In this paper, we consider a motion planning problem of a continuum of agents between successive equilibria at times  $t_i$ . The agents are described by their abscissa,  $x = 0$  (resp.  $x = 1$ ) designing the *left-most* (resp. *right-most*) agent. As in Meurer and Krstić (2011), we first consider our system as a continuum to solve the PDE and then discretize the solution to extract trajectories for the agents.

One of the problem arising in such models are the transitions between successive solutions. In Meurer and Krstić (2011) a new term, which is non-analytic at transition times  $t_i$ , is added to Burgers' equation to ensure smooth transitions between states. In the present paper we will instead look for non-analytic solutions of Burgers' genuine viscous equation so to allow infinite differentiability of the global solution at equilibria.

Using the Hopf-Cole transform  $u = -2\mu\phi_x/\phi$ , one transforms Burgers' viscous equation  $u_t + uu_x = \mu u_{xx}$ , where  $u$  denotes a spatial coordinate of the agent, into the standard heat equation  $\phi_t = \mu\phi_{xx}$ . As shown in the following proposition, if the solution of the heat equation is Gevrey of order  $\alpha$ , then the resulting solution to Burgers' equation is Gevrey of order  $\alpha$ .

*Proposition 1.* If  $\phi$  is Gevrey of order  $\alpha$  and if there exists  $c > 0$  such as  $\forall x \in [0, 1], \forall t \in [0, 1], \phi(x, t) > c$  then  $u = \phi_x/\phi$  is Gevrey of order  $\alpha$ .

**Proof.** Let  $v(x, t) = \ln \phi(x, t)$ . Since  $\ln$  is analytic on  $[c, \infty[$ , it is Gevrey of order 1. Hence  $v$  is Gevrey (see Yamanaka (1989)) and has same order as  $\phi$  as long as this order is greater than 1. Since  $u = v_x$ ,  $u$  is Gevrey and has same order as  $v$  and thus, as  $\phi$ .

Let us recall the following result due to Holmgren (1908):

*Proposition 2.* The heat equation with Cauchy boundary control in  $x = 0$  is flat.

**Proof.** Using the Laplace transform on the heat equation, we get  $s\hat{\phi}(x, s) = \mu\partial_x^2\hat{\phi}(x, s)$ . Solving this  $x$  ODE follows in the system:

$$\begin{cases} \hat{\phi}(x, s) = \hat{C}_x\hat{\lambda}_1(s) + \hat{S}_x\hat{\lambda}_2(s) \\ \hat{C}_x = \cosh(x\sqrt{s/\mu}), \hat{S}_x = \sqrt{\mu/s} \sinh(x\sqrt{s/\mu}) \end{cases}$$

Using the Laplace inverse transform, we get  $\phi(x, t) = C_x\lambda_1(t) + S_x\lambda_2(t)$  where  $C_x = \cosh(x\sqrt{\partial_t/\mu})$  and  $S_x = \sqrt{\mu/\partial_t} \sinh(x\sqrt{\partial_t/\mu})$  are differential operators of infinite order (see for example Van Tran and Dinh (1994)).

It is obvious that  $\partial_x C_x = \partial_t(S_x)/\mu$  and  $\partial_x S_x = C_x$ . Furthermore  $C_0 = 1$  and  $S_0 = 0$ . Deriving  $\phi$  according to  $x$  leads to  $\phi_x(x, t) = \partial_t/\mu(S_x\lambda_1(t)) + C_x\lambda_2(t)$ . We then get  $\lambda_1(t) = \phi(0, t)$  and  $\lambda_2(t) = \phi_x(0, t)$ .

Thus  $(\phi_0, \phi_{x,0})$  is a flat output of the system, where  $\phi_0$  (resp.  $\phi_{x,0}$ ) stands for  $\phi(0, t)$  (resp.  $\phi_x(0, t)$ ).

Instead of having two controls on one side, we use the following proposition to control the equation on both sides: *Proposition 3.* The heat equation with controls in  $x = 0$  and  $x = 1$  is flat.

**Proof.** For convenience we will set  $\mu = 1$ . Based on the result of the previous proposition, we may write the solution to the heat equation as:

$$\phi(x, t) = C_x\phi_0(t) + S_x\phi_{x,0}(t) \quad (1)$$

we thus have:

$$\phi(1, t) = C_1\phi_0(t) + S_1\phi_{x,0}(t) \quad (2)$$

Let us assume we may invert the  $S_1$  operator, equation (2) turns into:

$$\phi_{x,0}(t) = (S_1)^{-1}(\phi(1, t) - C_1\phi_0(t)) \quad (3)$$

This inversion is formal and no proof of its convergence is given. Injecting equation (3) in (1), we get:

$$\phi(x, t) = (C_x - T_x C_1)\phi_0(t) + T_x\phi_1(t) \quad (4)$$

where  $T_x$  stands for  $S_x(S_1)^{-1}$ . Thus, assuming the  $T_x$  operator has a meaning and has a sufficient regularity regarding the chosen controls, we get the result.

*Remark:* Since  $T_1 = 1, T_0 = 0$  and  $C_0 = 1$ , we may rewrite equation (4) in a symmetric way:

$$\phi(x, t) = (C_x T_1 - T_x C_1)\phi_0(t) - (C_x T_0 - T_x C_0)\phi_1(t)$$

Using the Taylor expansion of  $\text{csch}$  (Abramowitz and Stegun, 1965, p. 85), we get a formal expression of  $(S_1)^{-1}$ :

$$(S_1)^{-1} = \sum_{k \geq 0} u_k \frac{d^k}{dt^k}$$

where  $u_0 = 1$  and  $u_k = 2(1 - 2^{2k-1})B_{2k}/(2k)!$  where  $B_k$  is the  $k$ -th Bernoulli number. Thus, assuming expression (3) has a meaning, we get a formal expression of the  $T_x$  operator:

$$T_x = \sum_{k \geq 0} \left( \sum_{l=0}^k \frac{x^{2l+1} u_{k-l}}{(2l+1)!} \right) \frac{d^k}{dt^k} \quad (5)$$

We show in the following a meaning of this inversion.

*Remark:* Based on (Abramowitz and Stegun, 1965, p. 807),  $u_k = (-1)^{k+1} 4(1 - 2^{2k-1})\zeta(2k)/(2\pi)^{2k}$  where  $\zeta$  is the Riemann zeta function. Thus we get the asymptotic approximation  $u_k \sim 2(-1)^k/\pi^{2k}$ .

## 3. SOLUTION COMPUTATION

### 3.1 Control building

We consider the motion of a formation of  $N$  fully actuated UAV's between the times  $t_0 = 0$  and  $t_1 = 1$ . We describe the initial and final formation with the polynomials:

$$\begin{cases} f_0(x) = \sum_{i=0}^{2N-1} p_i \frac{x^i}{i!} = \sum_{i=0}^{2N-1} r_i \frac{(x-1)^i}{i!} \\ f_1(x) = \sum_{i=0}^{2N-1} q_i \frac{x^i}{i!} = \sum_{i=0}^{2N-1} s_i \frac{(x-1)^i}{i!} \end{cases} \quad (6)$$

Both functions interpolate their respective formation. Furthermore, we want in some cases the left-most and right-most agents going through a given set of points.

A way to find appropriate  $(p_i, q_i, r_i, s_i)$  regarding to the trajectories and formations constraints will be explained in appendix A.

Since  $f_0(x) = \phi(x, t = 0)$  and  $f_1(t) = \phi(x, t = 1)$ , by identification of the coefficients of the left- and right-hand sides in (1) and (6), we have the following conditions:

$$\begin{cases} \overbrace{\left\{ \begin{array}{l} \phi_0^{(i)}(0) = p_{2i} \\ \phi_0^{(i)}(1) = q_{2i} \\ \phi_{x,0}^{(i)}(0) = p_{2i+1} \\ \phi_{x,0}^{(i)}(1) = q_{2i+1} \end{array} \right\}}^{0 \leq i < N} & \overbrace{\left\{ \begin{array}{l} \phi_0^{(i)}(0) = 0 \\ \phi_0^{(i)}(1) = 0 \\ \phi_{x,0}^{(i)}(0) = 0 \\ \phi_{x,0}^{(i)}(1) = 0 \end{array} \right\}}^{i \geq N} \end{cases} \quad (7)$$

(resp. in  $x = 1$  with  $r_i$  and  $s_i$ ).

Based on the work in Laroche et al. (2000), we now propose trajectories for both left-most and right-most agent as:

$$\begin{cases} \phi_0(t) = \sum_{i=0}^{N-1} \left( p_{2i} \frac{t^i}{i!} (1 - \Phi(t)) + q_{2i} \frac{(t-1)^i}{i!} \Phi(t) \right) \\ \phi_1(t) = \sum_{i=0}^{N-1} \left( r_{2i} \frac{t^i}{i!} (1 - \Phi(t)) + s_{2i} \frac{(t-1)^i}{i!} \Phi(t) \right) \end{cases} \quad (8)$$

where  $\Phi(t)$  is a Gevrey function non-analytical (thus of order  $\alpha > 1$ ) in  $t = 0$  and  $t = 1$  with  $\Phi(0) = 0$  and  $\Phi(1) = 1$ . Since scaling, integration, addition, multiplication and composition of Gevrey functions of order  $\alpha > 1$  is of order  $\alpha$ , the latter proposed trajectories are Gevrey of order  $\alpha$ . We will write this as:

$$\begin{cases} \phi_0(t) = P_0(t)(1 - \Phi(t)) + Q_0(t)\Phi(t) \\ \phi_1(t) = R_0(t)(1 - \Phi(t)) + S_0(t)\Phi(t) \end{cases}$$

Considering the functions for  $t \leq 0$  and  $t \geq 1$ , we easily see that we achieve a  $C^\infty$  transition between two polynomials. Furthermore, the proposed solution verifies the condition (7) in  $\phi_0(t)$ . It verifies similar conditions for  $\phi_1(t)$  with  $r_{2i}$  and  $s_{2i}$ . We will show in the following it also verifies the conditions in  $\phi_{x,0}(t)$  and  $\phi_{x,1}(t)$ .

In the following, we will use the  $\Phi_\gamma(t)$  used in Laroche et al. (2000), where  $\gamma > 0$ :

$$\Phi_\gamma(t) = \begin{cases} 0 & \text{if } t \leq 0 \\ 1 & \text{if } t \geq 1 \\ \int_0^t \phi_\gamma(\tau) d\tau / \int_0^1 \phi_\gamma(\tau) d\tau & \text{if } t \in ]0; 1[ \end{cases}$$

where:

$$\phi_\gamma(t) = \begin{cases} 0 & \text{if } t \leq 0 \text{ or } t \geq 1 \\ \exp(-1/((1-t)t)^\gamma) & \text{if } t \in ]0; 1[ \end{cases}$$

The  $\phi_\gamma$  function (and thus the  $\Phi_\gamma$ ) is Gevrey of order  $1 + \frac{1}{\gamma}$  and non analytic in  $t = 0$  and  $t = 1$ .

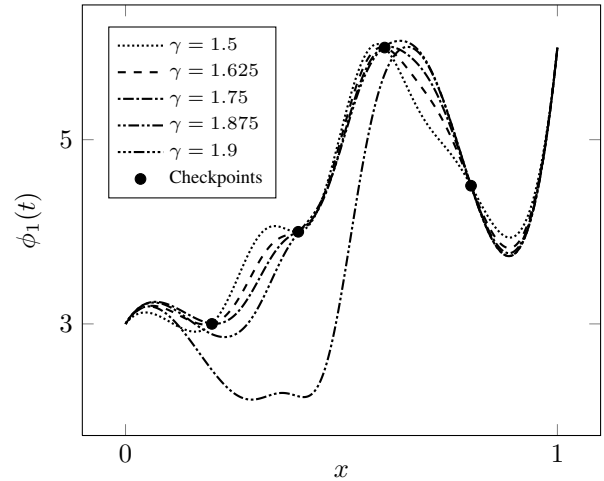


Fig. 1. Control in  $x = 1$

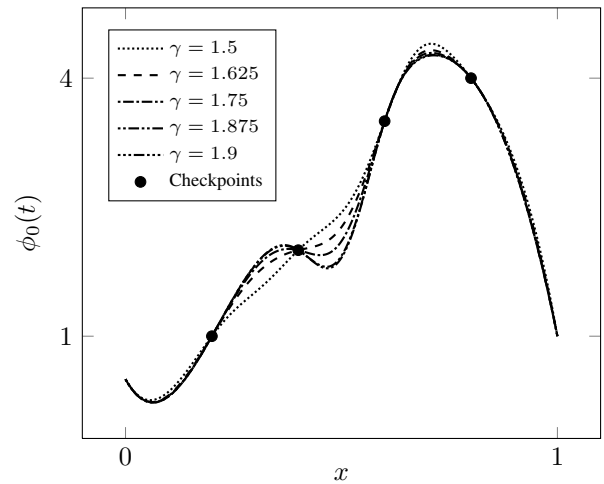


Fig. 2. Control in  $x = 0$

### 3.2 Control validation

It is straightforward to solve the heat equation numerically with given controls  $\phi_0$  and  $\phi_1$  and initial condition  $f_0$ .

On the one hand, as shown on figure 1 and 2, the bigger  $\gamma$ , the more “bumpy” the control is. In the same time, the bigger  $\gamma$ , the less the control follows exactly the checkpoints. Since controls are constructed to follow exactly the checkpoints, it is doubtlessly a matter of computational accuracy in the inversion of matrices in appendix A.

On the other hand, it also appears that the value of  $\gamma$  is of great meaning in order to conform to final formations. While  $\gamma$  decreases toward 0, the controls are more and more Gevrey divergent. While  $\gamma$  increases, the more the  $\Phi_\gamma$  function is a step at  $t = 1/2$  and thus the more the computational accuracy decreases. As shown by figure 3, accuracy increases toward  $\gamma = 1.685$  and decreases afterwards. For further applications, we use  $\gamma = 1.5$ , which allows reasonable respect of checkpoints and final formation.

A numerical solution to the heat equation with our controls is given in figure 4. Trajectories are given by  $x$  constant lines.



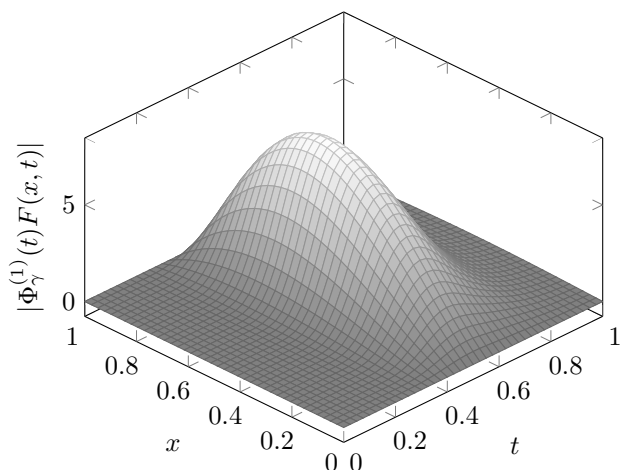


Fig. 5. Numerical evaluation of  $|\Phi_\gamma^{(1)}(t)F(x,t)|$  ( $\gamma = 1.5$ )

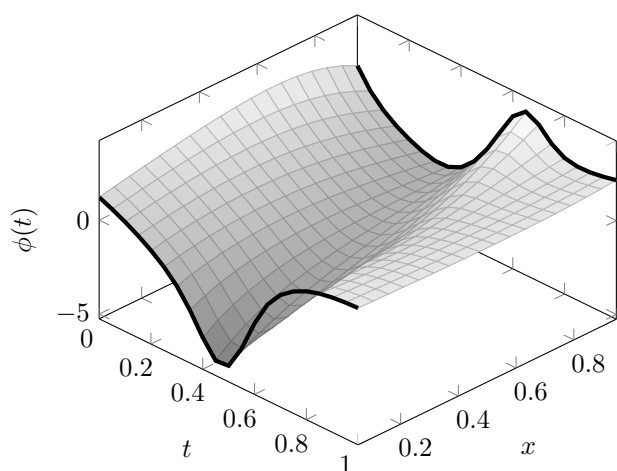


Fig. 6. Trajectories between constant states ( $\gamma = 1.5$ )

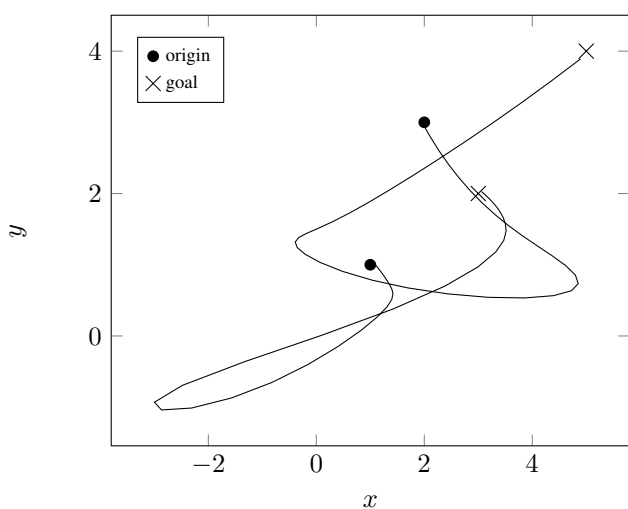


Fig. 7. Trajectories of two robots in a 2D plane ( $\gamma = 1.5$ )

#### 4. CONCLUSION

We have shown a way to solve Burgers' viscous equation using Gevrey functions allowing infinitely differentiable transitions between successive solutions. These solutions are used for motion planning for multi-agent systems.

Simulations are given while experiments using quadrotors are foreseen.

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## Appendix A

In this appendix, we show how to set the coefficients  $p_i$ ,  $q_i$ ,  $r_i$  and  $s_i$  so our system achieves the desired tasks. In a first part we propose a way to get trajectories adapted for the heat equation. In a second part we propose a way to get appropriate coefficients to solve Burgers' equation.

We write  $\mathbf{r}_0$  (resp.  $\mathbf{s}_0$ ,  $\mathbf{p}_0$ ,  $\mathbf{p}_1$ ,  $\mathbf{q}_0$  and  $\mathbf{q}_1$ ) the vector  $(r_{2i})$  (resp.  $(s_{2i})$ ,  $(p_{2i})$ ,  $(p_{2i+1})$ ,  $(q_{2i})$  and  $(q_{2i+1})$ ),  $F_0$  and  $F_1$  the upper-triangular matrices of generic terms  $1/(2(j-i))!$  and  $1/(2(j-i+1))!$ . Based on (6) we get the relations:

$$\mathbf{r}_0 = F_0 \mathbf{p}_0 + F_1 \mathbf{p}_1, \mathbf{s}_0 = F_0 \mathbf{q}_0 + F_1 \mathbf{q}_1 \quad (\text{A.1})$$

Let the respective index of every agent be  $i/(N-1)$ ,  $0 \leq i < N$ . Let  $\mathbf{d}^s = (d_i^s)$  (resp.  $\mathbf{d}^f = (d_i^f)$ ) be the initial (resp. final) formation, so that  $f_0(i/(N-1)) = d_i^s$  (resp.  $f_1(i/(N-1)) = d_i^f$ ). We write  $A$  the invertible Vandermonde matrix of generic term  $((i/N-1)^{2l})_{0 \leq i, l < N}$  and  $J_0$  (resp.  $J_1$ ) the diagonal matrix of generic term  $(1/(2i)!) (resp. (1/(2i+1)!))$  and  $H$  the diagonal non invertible matrix of generic term  $(i/(N-1))$ . We have:

$$AJ_0 \mathbf{p}_0 + HAJ_1 \mathbf{p}_1 = \mathbf{d}^s, AJ_0 \mathbf{q}_0 + HAJ_1 \mathbf{q}_1 = \mathbf{d}^f$$

Writing  $Q = J_0^{-1} A^{-1}$ , which is invertible and  $R = HAJ_1$  which is not, we get:

$$\mathbf{p}_0 = Q(\mathbf{d}^s - R\mathbf{p}_1), \mathbf{q}_0 = Q(\mathbf{d}^f - R\mathbf{q}_1) \quad (\text{A.2})$$

We also want the left trajectory (resp. right) going through points  $(e_i^0)_{0 \leq i < N}$  (resp.  $(e_i^1)_{0 \leq i < N}$ ) at time  $(t_i^0)_{0 \leq i < N}$

(resp.  $(t_i^1)_{0 \leq i < N}$ ). Since the positions of the left- and right-most agents at time  $t = 0$  and  $t = 1$  are already known, we take  $0 < t_i^0, t_i^1 < 1$ . Let  $t_i^0 = t_i^1 = (i+1)/(N+1)$ . Let  $P$  be the anti-diagonal matrix of generic term 1 (with  $PP = I$ ). Let  $\Phi$  be the diagonal matrix of generic term  $(\Phi_\gamma(t_i^0))_{0 \leq i < N}$ . Since  $\Phi_\gamma(1-t) = 1 - \Phi_\gamma(t)$ , we have  $(I - \Phi) = P\Phi P$ . Let  $V$  (resp.  $T$ ) be the Vandermonde matrix of generic term  $((t_i^0)^j)_{0 \leq i, j < N}$  (resp.  $((t_i^0 - 1)^j)_{0 \leq i, j < N}$ ). Let  $B$  be the diagonal matrix of generic term  $((-1)^i)_{0 \leq i < N}$  (notice we have  $BB = I$ ). Since  $t_i^j = 1 - t_{N-1-i}^j$ ,  $j \in \{0, 1\}$ , we have  $V = PTB$ . Let  $G$  be the diagonal matrix of generic term  $(1/(i!))_{0 \leq i < N}$ . We get, using equation (8):

$$\begin{cases} \mathbf{e}^0 = P\Phi PVG\mathbf{p}_0 + \Phi PVGB\mathbf{q}_0 \\ \mathbf{e}^1 = P\Phi PVG\mathbf{r}_0 + \Phi PVGB\mathbf{s}_0 \end{cases} \quad (\text{A.3})$$

Using relation (A.1) in the latter and writing  $D = P\Phi PVG$  and  $E = \Phi PVGB$  (which are both invertible matrices), we get:

$$\begin{cases} \mathbf{e}^0 = D\mathbf{p}_0 + E\mathbf{q}_0 \\ \mathbf{e}^1 = D(F_0\mathbf{p}_0 + F_1\mathbf{p}_1) + E(F_0\mathbf{q}_0 + F_1\mathbf{q}_1) \end{cases} \quad (\text{A.4})$$

Using equations (A.2) in the previous equations, writing  $\hat{Q} = Q^{-1}D^{-1}$  and  $\tilde{Q} = Q^{-1}F_0^{-1}D^{-1}$  – which are both invertible – we get the global system:

$$\begin{cases} \mathbf{p}_0 = Q(\mathbf{d}^s - R\mathbf{p}_1), \mathbf{q}_0 = Q(\mathbf{d}^f - R\mathbf{q}_1) \\ \hat{Q}\mathbf{e}^0 = \mathbf{d}^s - R\mathbf{p}_1 + K(\mathbf{d}^f - R\mathbf{q}_1) \\ \tilde{Q}\mathbf{e}^1 = \mathbf{d}^s - R\mathbf{p}_1 + \tilde{Q}DF_1\mathbf{p}_1 + L_0(\mathbf{d}^f - R\mathbf{q}_1) + L_1\mathbf{q}_1 \end{cases}$$

Where  $K = \hat{Q}EQ$ ,  $L_0 = \tilde{Q}EF_0Q$  and  $L_1 = \tilde{Q}EF_1$ , are invertible matrices. Subtracting the third line to the fourth, we get:

$$\begin{cases} \mathbf{p}_0 = Q(\mathbf{d}^s - R\mathbf{p}_1), \mathbf{q}_0 = Q(\mathbf{d}^f - R\mathbf{q}_1) \\ \hat{Q}\mathbf{e}^0 = \mathbf{d}^s - R\mathbf{p}_1 + K(\mathbf{d}^f - R\mathbf{q}_1) \\ \tilde{Q}DF_1\mathbf{p}_1 = \tilde{Q}\mathbf{e}^1 - \tilde{Q}\mathbf{e}^0 + (K - L_0)\mathbf{d}^f + ((L_0 - K)R - L_1)\mathbf{q}_1 \end{cases} \quad (\text{A.5})$$

Then, injecting the fourth line in the third, we get an expression of  $\mathbf{q}_1$  depending only on  $\mathbf{e}^0$ ,  $\mathbf{e}^1$ ,  $\mathbf{d}^s$  and  $\mathbf{d}^f$ . Assuming the matrix  $RF_1^{-1}D^{-1}\tilde{Q}^{-1}((L_0 - K) - L_1) + KR$  is invertible, we get an exact expression of  $\mathbf{q}_1$ . Using the three other equations, we get the three other vectors.  $\mathbf{r}_0$ ,  $\mathbf{r}_1$ ,  $\mathbf{s}_0$  and  $\mathbf{s}_1$  are then found using equations (A.1).

In the case of Burgers' equation, we have to use the Hopf-Cole transform. Since no simple expression of  $F(x, t)$  is yet known, one can only set the positions for initial and final formations where an explicit polynomial expression is known. In this case, writing the desired positions as  $\mathbf{u}_0$  and  $\mathbf{u}_1$ , we have to solve the system :

$$AJ_0\mathbf{p}_1 + HAJ_1D\mathbf{p}_0 = \mathbf{u}_0, AJ_0\mathbf{q}_1 + HAJ_1D\mathbf{q}_0 = \mathbf{u}_1$$

where  $D$  is the derivation matrix (all but the first upper diagonal are filled with zeros). In this case  $\mathbf{d}^s$  and  $\mathbf{d}^f$  are degrees of freedom and are used through optimization to achieve, in our implementation, trajectories of minimal amplitude.