



## Modelling of flawed riveted structure for EC inspection in aeronautics

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## Context and objective

- The industrial demand is to detect efficiently flaws located nearby a fastener
- ✓ Need of Eddy Current inspection for flawed fastened structure



- Development of a semi-analytical model in CIVA
- ✓ Based on the Volume Integral Method
- ✓ Handles a multi-layer structure



## The semi-analytical model

The state equation

$$\mathbf{E}_k(\mathbf{r}) = \mathbf{E}_k^{(0)}(\mathbf{r}) - j\omega\mu_0 \sum_{l=m}^n \int_{\Omega_l} \bar{\mathbf{G}}_{kl}^{(ee)}(\mathbf{r}, \mathbf{r}') [\sigma_l - \sigma(\mathbf{r}')] \mathbf{E}_l(\mathbf{r}') d\mathbf{r}'$$

Primary field in the layer  $k$       Dyadic Green's functions

Linear system from state equation ( $MoM$ ) Solved by Matrix inversion or Iterative resolution

$$\begin{bmatrix} \mathbf{E}_m^{(0)} \\ \vdots \\ \mathbf{E}_n^{(0)} \end{bmatrix} = \left( \mathbf{I} - \begin{bmatrix} \mathbf{G}_{m,m} & \cdots & \mathbf{G}_{m,n} \\ \vdots & \ddots & \vdots \\ \mathbf{G}_{n,m} & \cdots & \mathbf{G}_{n,n} \end{bmatrix} \right) \begin{bmatrix} \mathbf{E}_m \\ \vdots \\ \mathbf{E}_n \end{bmatrix}$$

 $G_{i,i}$  electromagnetic self-coupling terms of the  $i^{th}$  region onto itself $G_{i,j}$  mutual coupling terms of the  $j^{th}$  region over the  $i^{th}$ 

Theoretical Formulation

The dyadic Green's functions are solution of

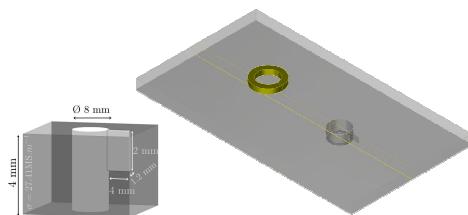
$$\nabla \times \nabla \times \bar{\mathbf{G}}_{kl}^{(ee)}(\mathbf{r}, \mathbf{r}') - k_k^2 \bar{\mathbf{G}}_{kl}^{(ee)}(\mathbf{r}, \mathbf{r}') = \delta_{kl} \bar{\delta}(\mathbf{r} - \mathbf{r}')$$

The response of the probe is obtained via the reciprocity theorem

$$I_0^2 \Delta Z = \sum_{l=m}^n \int_{\Omega_l} [\sigma_l - \sigma(\mathbf{r})] \mathbf{E}_l^{(0)}(\mathbf{r}) \cdot \mathbf{E}_l(\mathbf{r}) d\mathbf{r}$$

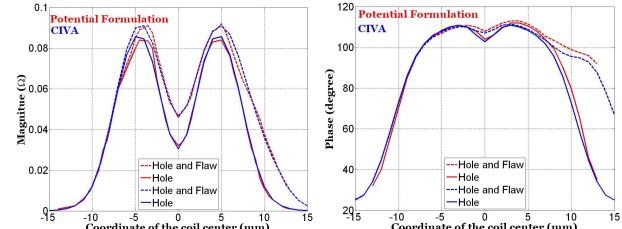
where  $I_0$  is the feeding current of the probe,  $\Omega$  the calculation volume and  $\sigma$  the conductivity

## Configuration Zeng & al (ACES'07)



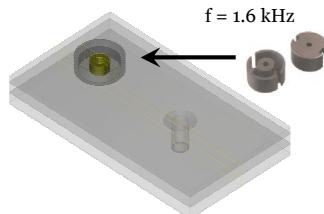
**Good agreement**  
with the data published in  
“Reduced Magnetic Vector  
Potential and Electric Scalar  
Potential Formulation for Eddy  
Current Modeling”

Z. Zeng &amp; al

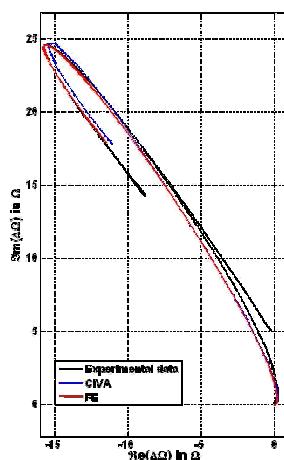


## Validation on an aeronautical configuration

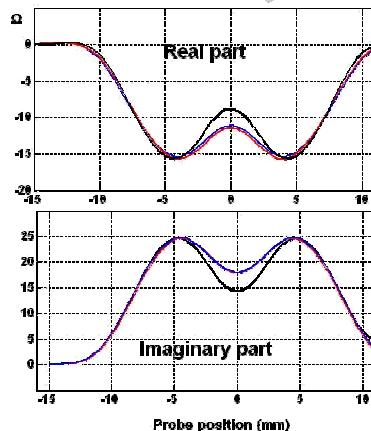
**calibrated Rivet**  
**Calibration**  
CIVA : 1.3 +4°  
LGEP: 1.06 -1°



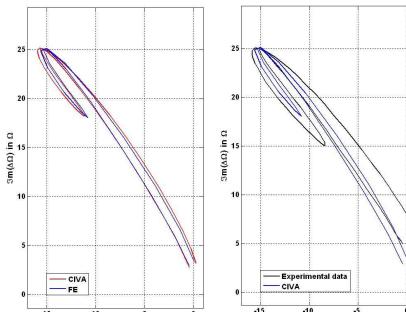
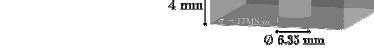
**Flawed Rivet**



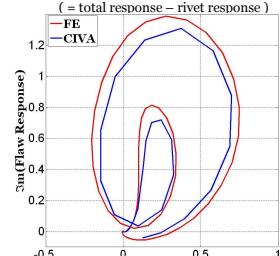
Real part



Imaginary part



Flaw response



Validation with experimental data is more difficult to achieve because of

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## Conclusion

- Comparison with published data (Zeng & al configuration)  
Good agreement with the Potential Formulation
- Validation with experimental data (aeronautical configuration)  
Good agreement with FE once calibrated, exhibiting Typical signature of the flaw in simulations

## Perspectives

- Optimization of the discretization in order to improve the simulation of a flawed rivet  
Best efficiency of the method
- Simulation of other rivet inspection techniques