

# Maximum power point analysis for partial shading detection and identification in photovoltaic systems

Siwar Fadhel, Demba Diallo, Claude Delpha, Anne Migan-Dubois, I. Bahri,

Mohamed Trabelsi, Mohamed Faouzi Mimouni

# ▶ To cite this version:

Siwar Fadhel, Demba Diallo, Claude Delpha, Anne Migan-Dubois, I. Bahri, et al.. Maximum power point analysis for partial shading detection and identification in photovoltaic systems. Energy Conversion and Management, 2020, 224, pp.113374. 10.1016/j.enconman.2020.113374 . hal-02938015

# HAL Id: hal-02938015 https://centralesupelec.hal.science/hal-02938015v1

Submitted on 14 Sep 2022

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers. L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Distributed under a Creative Commons Attribution - NonCommercial 4.0 International License

# Maximum Power Point Analysis for Partial Shading Detection and Identification in Photovoltaic Systems

3 4	S. Fadhel <sup>1,2,4</sup> , D. Diallo <sup>2</sup> , C. Delpha <sup>3</sup> , A. Migan <sup>2</sup> , I. Bahri <sup>2</sup> , M. Trabelsi <sup>4</sup> , M.F. Mimouni <sup>4</sup>
5	<sup>1</sup> Université de Sousse, Ecole Nationale d'Ingénieurs de Sousse, 4023, Sousse, Tunisie
6 7	<sup>2</sup> Université Paris- Saclay, CentraleSupélec, CNRS, Laboratoire Génie Electrique et Electronique de Paris, 91192, Gif-sur-Yvette, France
8 9	<sup>3</sup> Université Paris- Saclay, CNRS, CentraleSupélec, Laboratoire des Signaux et Systèmes, 91192, Gif-sur-Yvette, France
10 11	<sup>4</sup> Ecole Nationale d'Ingénieurs de Monastir, Laboratoire Automatique, Systèmes Électriques et Environnement, 5035 Monastir, Tunisie
12	

#### 13 Abstract

14 Fault diagnosis of photovoltaic (PV) systems is a crucial task to guarantee security, increase productivity, efficiency, and availability. In this regard, numerous diagnosis methods have been 15 16 developed. Methods requiring the interruption of power production are not adequate for economic reasons. The development of large-scale PV plants and the objective of maintenance cost reduction 17 18 push toward the emergence of automatic on-line diagnosis methods that use available information. In this study, we propose two data-driven methods for partial shading diagnosis using only the maximum 19 power point's information. It does not require the interruption of production, nor does it require any 20 additional equipment to obtain the I(V) curve. The analyses are conducted with principal component 21 22 analysis (PCA) and linear discriminant analysis (LDA) to detect and classify the faults. The experimental dataset is collected from a 250 Wp PV module under four states of health (healthy, and 23 three severities of partial shading) for several meteorological conditions. The classification results 24 have a 100% success rate, and are robust to the variations of temperature and irradiance. 25

26 Keywords: Photovoltaic system, Fault diagnosis, Partial shading, Maximum Power Point (MPP),

27 Principal Component Analysis, Linear Discriminant Analysis

28

#### 1. Introduction

Although photovoltaic (PV) cells/modules are the most reliable components in a PV installation [1] and considered as systems with low failure rates [2] requiring low maintenance [3], it is crucial to implement effective monitoring systems for PV modules to diagnose their state of health. Indeed, many PV faults can cause significant power losses, may lead to accelerated system ageing, reduced efficiency, and even safety hazards.

Due to uncertainties related to PV cell technology, manufacturing process and climatic conditions, 37 correlating PV fault type to power loss is tricky. It is still an on-going area of research. In particular, 38 the impact of climatic conditions is evaluated in [4], [5] by studying a large number of PV modules 39 40 exposed to different climates. The annual degradation rate is proposed by numerous studies to quantify 41 the impact of single or multiple faults. For example, it has been reported that crystalline silicon (c-Si) PV modules have degraded at an annual rate of approximately 7% due to discoloration and weakened 42 solder bonds [6]. Another study reported that because of discoloration, the power loss could reach 43 10% per year in PV modules with concentrators [5]. According to [4], PV installations deployed after 44 45 the 2000s are more susceptible to the occurrence of defects. However, the percentage of degradation 46 would be significantly lower than in previous installations. In particular, for new c-Si PV modules, the 47 biggest concern seems to be hot spots, followed by potential induced degradation (PID). Hot spots have an impact on PV module performance and could contribute to premature ageing if they are 48 49 frequent [7]. It has also been reported that partial shading (PS) can lead to several early degradations, 50 and is a significant cause of the appearance of hot spots. Therefore, we are interested in partial shading (PS) diagnosis. 51

52 Several PV faults have a visual signature such as delamination, burn, or discoloration marks. So,
53 they can be simply detected through visual inspection. This technique is clearly irrelevant for large PV
54 installations. Moreover maintenance policies are evolving towards Condition Based Maintenance

(CBM) to prevent failures and reduce maintenance costs. CBM requires continuous monitoring and
automatic fault diagnosis methods.

57 There are several methods for diagnosing PV faults, reviewed in the literature [8] to [11]. They can
58 be classified into two main families according to the measures used:

- 59 The first group uses radiation-based techniques: Electroluminescence (EL) [12], [13], and Infrared Thermography (IRT) under steady-state conditions [13], [14]. The main advantage of 60 these techniques is their ability to detect and locate the faults in real-time. EL is generally 61 performed to detect micro-cracks in PV cells and other faults within the cell material (contact 62 63 degradation...); however, it requires the system interruption. IRT can be performed at module level, allowing a fast and effective inspection to detect different types of faults. This 64 technique can be tested without any operational interruption, but it requires mobile platforms 65 to diagnose many PV modules. For this reason, researches are ongoing to develop advanced 66 67 IRT techniques such as drone-mounted thermography [15]. Therefore, IRT could be more suitable than the EL technique, especially for big PV plants. 68
- The second group uses electrical measures. It is composed of reflectometry techniques, I(V)
   curve analysis, and maximum power point (MPP) coordinates analysis.

Reflectometry techniques are mainly used to detect catastrophic faults (ground faults and arc faults)
and locate open-circuit faults in the PV strings. These methods are effective. Nevertheless, they are
costly since they require a specific external signal function generator to stimulate the PV system [16]–
[20].

I(V) curves can also be used for fault diagnosis. However, not only do several defects have very similar signatures, but the I(V) curve is also very sensitive to environmental conditions. Therefore diagnosis methods based on the analysis of the entire I(V) curve's points need appropriate

preprocessing. This difficulty may be one of the reasons that justify the limited number of publications 78 79 using the full I(V) curve for fault diagnosis. From the literature review, we have only found two 80 studies dealing with the full I(V) curve analysis for diagnosis purposes [7], [23]. In [7], the analysis of the first derivative of the ratio between the standard error and the PV voltage is used for the same 81 fault, the standard error results from the comparison between faulty and healthy I(V) data. Authors in 82 [23] have proposed the evaluation of the first and the second derivatives of the curve for shading 83 detection. An I(V) plotter has been used in this study to sweep the I(V) curve composed of 265 points. 84 85 We have proposed in two previous works a new method based on the full I(V) curve analysis to detect and classify shading faults by using adequate variables [21], [22]. The experimental I(V) 86 characteristics are obtained thanks to a programmable voltage source, which provides the points from 87 the short-circuit current to the open-circuit voltage. 88

The other diagnosis techniques use the actual I(V) curve to extract several health indicators from the shape of the curve. The fault diagnosis decision is made upon analysis of the residuals computed as differences between measured indicators and estimated ones identified from the healthy I(V)characteristics. This latter is generally obtained by considering the usual electrical equivalent circuit model (single-diode or double-diode) [24]. At first, an optimization algorithm is applied to extract the five optimal parameters, as proposed in [25]–[29]. Then, the non-linear equation I = f(V) is solved iteratively to reproduce the healthy behavior of the PV system.

In [30], the authors have defined five indicators (fill factor, equivalent series resistance...) calculated from the shape of the outdoor measured on-line I(V) curve. Fault occurrence is detected by comparing the actual values with their initial values measured during the commissioning phase of the diagnosis system. Based on the one-diode model, authors in [31] have defined two reference indicators to estimate the increment of the series resistance from the measures of the short-circuit current  $I_{SC}$ , PV system temperature  $T_{PV}$ , maximum power point's voltage and current. The experimental indicators analysis is performed with a variable load used to extract the full I(V) curve. These methods suffer from several difficulties. First, they introduce additional time to sweep the full I(V) characteristic, and the duration and the quality of acquisition depend on the used instrument. Second, these approaches are confronted with the case of large-scale photovoltaic plants with limited measurements. Furthermore, it is not practical to disconnect PV modules or strings to extract their I(V) curves as it perturbs the system operation and leads to production losses. For instance, the power loss due to the I (V) acquisition in [32] resulted in a power efficiency drop of 0.16%.

For this reason, it is not suitable for continuous monitoring. There is therefore, an interest in using methods that do not require the interruption of production and that use only available data such as voltage and current at the point of maximum power (MPP) commonly available in PV systems. This approach is also cost-effective, as it does not require any additional measurement equipment.

The fault detection strategy developed in [33] is based on monitoring only the maximum power of 113 the PV system by analyzing the sample entropy. In [34], authors have proposed two diagnosis 114 attributes, which are the voltage ratio (VR) and power ratio (PR) computed from the division of the 115 theoretical and the measured values of the maximum power point's voltage and power, respectively. 116 117 More recently, to distinguish healthy from faulty states, three diagnosis indicators calculated from the comparison between predicted and measured current, voltage, and power at MPP have been proposed 118 in [26]. The same electrical measurements are exploited in [35], [36], to define three residuals as fault 119 120 features. The data in these two studies are recorded from the same PV system whose behavior in the 121 healthy state is estimated based on the one-diode model. Residuals are analyzed with the one-class support vector machine (1SVM) technique in [35], while the exponentially weighted moving average 122 123 (EWMA) approach is applied to the same residuals in [36], to detect and identify the faults. All the previous analysis methods using the maximum power point's coordinates rely on physics-based 124 125 models. These methods are powerful in detecting many types of PV faults and can be applied to a 126 wide range of PV plants. However, they rely on an analytical model to reproduce the nominal PV characteristics, and an optimization process is implemented for parameter extraction. Subsequently, 127

MPP's coordinates in a healthy state are estimated under real climatic conditions. When dealing with large PV plants, the modeling stage can be quite challenging to reproduce the MPP's coordinates with high accuracy. Besides, due to the sensitivity of PV systems to weather conditions, optimal thresholds must be selected for effective and robust detection. Moreover, physics-based models need to be updated to take into account the natural ageing and degradation of solar cells. Unfortunately, these mechanisms are not yet well known in order to develop reliable models. Data-driven methods based on historical data could be a valuable alternative for PV fault diagnosis.

To the best of our knowledge, fault detection based on data-driven approaches using only real data at Maximum Power Point (MPP) data has not been well addressed; only one publication has been found in the literature [3]. Authors have proposed graph-based semi-supervised learning for fault diagnosis. The method is able to detect and identify line-to-line and open-circuit faults efficiently, but it is not suitable for partial shading detection.

140 It should be remembered that partial shading (PS) is responsible for several early degradations, and 141 is an essential cause of the appearance of hot spots. That is why, in what follows, we focus on the 142 diagnosis of partial shading (PS) using a methodology based on maximum power point data.

- 143 The methodology is based on four steps:
- Modelling step in which the data is collected from an experimental PV module of 250 Wp,
- Preprocessing step in which the variables (voltage, current, and power at the maximum
  power point) are selected, centered, reduced and processed through the logarithmic
  function,
- Features extraction: in this step two statistical techniques, principal component analysis
  (PCA) and linear discriminant analysis (LDA) are applied.

Features analyses: in this step, PCA and LDA are used for partial shading faults detection
and classification. LDA is also used to determine discriminative laws for data separation.

We will evaluate the robustness of the method to environmental conditions: variable temperatureand irradiation.

The outline of the paper is as follows: section 2 describes how the database is collected and extended. The detailed faults diagnosis methodology based on maximum power point (MPP) coordinates are presented in section 3. A case study of an isolated PV module is presented to validate the proposed methods. Section 4 discusses the application to large-scale PV plants and compares its practical implementation with full I (V)-based diagnosis technique. Finally, section 5 concludes the paper.

160 161

162

#### 2. Description of the dataset

#### *2.1.Data acquisition within a 15-minute time window*

The experiments were carried out on March 21, 2019, using the experimental setup displayed in Fig. 1. The main parameters of this module at standard test conditions (STC) are as follows [22]: the maximum power  $P_{mpp} = 250$  Wp, the maximum power current  $I_{mpp} = 8.21$  A, the maximum power voltage  $V_{mpp} = 30.52$  V, the short-circuit current  $I_{sc} = 8.64$  A, the open-circuit voltage  $V_{oc} = 37.67$  V. The temperature of the PV module  $T_{PV}$  is measured with a 4-wire Pt100 probe bonded on its back face.





Fig. 1. Installed PV panel platform



173 A reference cell (SOLEMS RG100) is used to measure G<sub>POA</sub> the plane of array irradiance.

The acquisition, display, and saving of each I (V) characteristic take one minute. Therefore, during 15 minutes, 15 experimental I(V) curves for each health status (healthy and the different shading profiles) are recorded for several levels of temperature  $T_{PV}$  and irradiance  $G_{POA}$ . Each curve is composed of 101 points. As an example, for the environmental conditions  $T_{PV}$  and  $G_{POA}$  presented in Fig. 2, the characteristics I(V) and P(V) under healthy status are displayed in Fig. 3. We can observe that due to the temperature and irradiance fluctuations (( $\Delta G_{POA}$ )max = 25% and ( $\Delta T_{PV}$ )max = 13%), the maximum power fluctuates from 149 Wp to 190 Wp.



Fig. 2. Module temperature and irradiance variations for a healthy PV module



Fig. 3. Measured I(V) and P(V) curves for a healthy PV module

The shading profiles as in [22], and the corresponding experimental I(V) and P(V) curves are displayed in Fig. 4. One can notice the maximum power drop caused by the bypass diodes activation. The solar irradiance and the module temperature measured during the partial shading experiments are plotted in Fig. 5. The maximum relative variations of irradiation and temperature are summarized in Table 1.

<sup>189</sup> Table 1. Maximum relative variations of irradiance and temperature

Partial Shading Condition	$\Delta(G_{POA})$ max (%)	$\Delta(T_{PV})$ max (%)
1	36	18.5
2	6	32
3	16	4.5







(b) Partial shading 2



Fig. 4. Partial Shading profiles and measured I (V) and P (V) curves





(c) Partial Shading 3



Fig. 5. Module temperature and irradiance variations for the different partial shading conditions

## 202 2.2. Extension of the database

203

To increase the number of points in the database, we have generated new I(V) curves from the experimental ones by varying the solar irradiance. In the following, we have doubled the number of points; from the original 15 maximum power points for each health status, we have now 30 points. Therefore, for the four modes (one healthy state and three partial shading ones), we have 30\*4 MPP observations. Experimental and generated I(V) curves are plotted respectively with blue and red colors in Fig. 6. 210 It must be noticed that MPP coordinates are almost always available in PV plants under operation,





- *The modelling*: For this step, we have chosen a data-driven model based on the 120 maximum
   power point coordinates extracted from the I (V) curves.
- Data pre-processing: This step is decisive for the performance level of the diagnostic method.
   It consists in choosing the field of information, the descriptive variables, and in implementing
   any technique allowing to keep the information useful and to eliminate nuisances. In our
   study, we used data from the maximum power point in the time domain, to which we applied
   the logarithmic function as in [22].
- 230 Features extraction and analysis: The third and fourth steps aim to extract from the • 231 maximum power points, the features (signatures) to be analyzed to detect, isolate, and estimate the fault severity. One of the difficulties lies in choosing the most efficient tools for 232 233 the extraction and analysis of signatures, especially since in our case the data varies with the 234 environmental conditions. This sensitivity makes it difficult to distinguish the healthy state from the faulty ones. Therefore, to ensure reliable fault detection, the most appropriate tool 235 236 should have the highest ability to separate the data from different health status. In this work, we have selected PCA and LDA for features' extraction and analysis to perform the PS 237 detection and classification. 238



Fig. 7. Flowchart of the four-step diagnosis methodology

239 240

# 242 *3.1.Review of normalization methods in the field of PV*

When dealing with maximum power point (MPP) in outdoor conditions, it might not be easy to 243 distinguish healthy status from shading ones. The maximum power point's coordinates change rapidly 244 due to variations in environmental conditions, and it becomes then difficult to differentiate whether a 245 fault or climatic changes cause the MPP variation. In other words, the faulty PV system may have 246 similar MPP's coordinates as a healthy one. Besides, the fluctuation of MPPs for different fault types 247 may be the same. This is confirmed by the evolutions of the maximum power points' coordinates 248 249 plotted in Fig. 8. For the current at MPP, Impp, we can observe the overlapping of several points in healthy conditions, partial shading 1, and partial shading 2. For the power at the MPP, P<sub>mpp</sub>, the 250 overlapping is observed in healthy conditions, partial shading 1, and partial shading 3. These overlaps 251 can be expected to be more pronounced when the data acquisition interval is greater. Therefore, to 252

ensure reliable fault detection, one should find appropriate processing techniques that highlight thedata's separability.





Fig. 8. Overlapping MPP's coordinates over a wide range of temperature and irradiance

Several methods of normalization have been proposed in the literature to mitigate the effect of the 258 259 environmental changes. Authors in [3] have defined two normalized parameters. The first one is the 260 ratio of MPP's voltage by the reference open circuit voltage multiplied by  $N_{\rm mod}$ , the number of series-261 connected PV modules. The second is the ratio of MPP's current by the reference short-circuit current  $I_{sc}$  ref multiplied by  $N_{Str}$  the number of parallel strings in the array. This technique is easy to 262 263 integrate within a PV inverter whatever its topology. However, it requires the use of two additional modules identical to the PV modules under test. They are considered as modules of reference to 264 measure instantaneous  $I_{sc}$  ref and  $V_{oc}$  ref with respect to solar irradiance and module temperature. 265 This normalization is efficient for detecting and classifying line-to-line and open-circuit fault, but it 266 cannot be used for partial shading. However, the main issue with this method is to guarantee that the 267 268 modules under test, and the modules of reference are in the same conditions of temperature and irradiance. Another normalization method is proposed in [33]. The PV array current, and voltage, are 269 270 divided by the STC short-circuit current, and the STC open-circuit voltage, respectively to calculate the normalized parameters, used to determine the entropy of the PV array output power. The method is 271

272 fast and effective for fault detection, however fault classification has not been considered. A per-unit 273 standardization has been applied in two recent studies [29], [40]. This normalization requires accurate 274 measurements of temperature and irradiance. It also assumes that the temperature coefficients of 275 voltage and current are constant. Nevertheless, several experiments on the PV modules installed at the 276 French observatory SIRTA have revealed that these coefficients vary depending on the meteorological 277 data. Based on this normalization, the diagnosis method in [40] achieved high fault identification 278 percentages for all the studied faults except for partial shading. In that case, the rate of correct identification is 53.66%, which is quite low. 279

Table 2 summarizes the normalization methods discussed above and the data size used to evaluateeach diagnosis approach.

282 Table 2. Normalized expressions used for PV system diagnosis to mitigate the climatic conditions effect

Variable	Normalized expression	Size of PV data	Reference
		Simulation test :	
	I	5576 MPP data	
Normalized current and voltage at MPP	$I_{mppn} = \frac{I_{mpp}}{N_{str} \times I_{sc\_ref}}$	1.43% used for training	[3]
-	$V = \frac{V_{mpp}}{V_{mpp}}$	Experimental test:	
	$N_{ m mod} \times V_{oc\_r\acute{e}f}$	5000 MPP data	
		1% used for training	
Normalized current	$I_{mppn} = \frac{I_{mpp}}{I_{sc0}}$	No training step	[33]
and voltage at MPP	$V_{mppn} = \frac{V_{mpp}}{V_{oc0}}$		

Per unit normalization of	$I_{mppn} = \frac{I_{mpp}}{I_{mpp0}} \frac{G}{1000} [1 + \alpha \frac{I_{mpp0}}{I_{sc0}} (T - 25)]$	123 I-V data 123/3 used for training	
Current and voltage at MPP, ideality factor, open-circuit voltage and short- circuit current.	$V_{nppn} = \frac{V_{npp}}{V_{npp0}} [1 + \beta \frac{V_{mpp0}}{V_{oc0}} (T - 25)]$ $I_{scn} = \frac{I_{sc}}{I_{sc0}} \frac{G}{1000} [1 + \alpha (T - 25)]$ $V_{ocn} = \frac{V_{oc}}{V_{oc0}} [1 + \beta (T - 25)]$		[40]
Per unit normalization of Current and voltage at MPP, ideality factor, open-circuit voltage and short- circuit current.	$n_n = \frac{n}{n_0} [1 + \alpha(T - 25)]$	<u>Simulation test :</u> 4800 I-V data 75% used for training <u>Experimental test :</u> 2500 I-V data 75% used for training	[29]

# 284 3.2. Feature Extraction and Analysis with Principle Component Analysis

In our case, before applying PCA, the three variables,  $I_{mpp}$ ,  $V_{mpp}$ , and  $P_{mmp}$  are centred (zero mean), and reduced (unit variance). The challenge is also to deal with a limited number of samples (thirty points per health status). The robustness of our proposal to  $T_{PV}$  and  $G_{POA}$  variations will be evaluated.

289 *3.2.1. Principle* 

The details of PCA are given in [22]. Briefly, PCA is a multivariate unsupervised technique that uses a linear combination of *m* original variables to create a low-dimensional set of new variables named principal components (PCs). The new variables are uncorrelated, and the new dataset is considered optimal when the variance of the information is maximal despite the reduction in the size of the representation space. The original data is arranged in a matrix  $X_{[N \times m]}$  where *N* represents the number of measurements/ observations for each of the *m* variables. The observations include data on healthy and faulty operating conditions. In the following, the PCA algorithm is applied to the matrix  $X = \log[V_{mpp} \quad I_{mpp} \quad P_{mpp}]$ .

298

# 3.2.2. Results in the training stage with the PCA algorithm

In the training step, 80 observations representing 67% of the dataset is used. The PCA is 299 applied to the matrix  $X_{[80\times3]} = \log[V_{mpp} \quad I_{mpp} \quad P_{mpp}]$ . We obtain three principal components PCi (i = 300 301 1,2,3), among which PC1 and PC2 preserve 99.9% of the initial total variance. The data can be 302 projected in four different sub-spaces spanned by PC1-PC2, PC1-PC3, PC2-PC3, or PC1-PC2-PC3 respectively. The projections of the training data are displayed in Fig.9. Except in the subspace 303 304 spanned by PC2 and PC3 (there is less information in PC2, and PC3 compared to PC1), the four classes can be clearly distinguished in the other three subspaces: one healthy class C0 and three faulty 305 ones noted C1, C2, and C3 (Table 3). The dispersion of the operating points found in the same group 306 307 is due to the climatic conditions variations. Table 4 summarizes the percentages of classification, and 308 shows that all the data samples are correctly classified. In this table, we also present the classification 309 performance when using all the points of the I(V) curve in [22]. Despite the variations of T<sub>PV</sub> and GPOA, and using only MPP's coordinates, the classification obtained in the present study is more 310 311 accurate with 100% rate of classification.

312

Table 3. The four health status classes

Test condition	Class
Healthy	$C_0$
Shading 1	$\mathbf{C}_1$
Shading 2	$C_2$
Shading 3	$C_3$





Fig. 9. Projection of the training Maximum Power Points' coordinates in the PCA subspaces

A priori Class				A poste	riori clas	S		
	Class	$C_0$	Class	C <sub>1</sub>	Class	C <sub>2</sub>	Class	C <sub>3</sub>
	MPP	I (V)	MPP	I (V)	MPP	I (V)	MPP	I (V)
Class C <sub>0</sub>	100	97.03	0	0	0	2.97	0	0
Class C <sub>1</sub>	0	0	100	98.52	0	1.48	0	0
Class C <sub>2</sub>	0	12.62	0	0	100	87.38	0	0
Class C <sub>3</sub>	0	0	0	0	0	0	100	100

Table 4. Confusion matrix for training dataset classification

# *3.2.3. Results in the validation stage with the PCA algorithm*

The remaining 33% of the database is used to test the effectiveness of the trained PCA model. The

321 test matrix is  $X_{[40\times3]} = \log[V_{mpp} \quad I_{mpp} \quad P_{mpp}]$  where 10 test samples are used for each health status. The

projections of the data in the subspaces spanned by the principal components obtained in the training stage are displayed in Fig.10. The classes related to partial shading 1, 2, and 3 are clearly separated from the healthy one with a classification rate of 100%. These results are also compared with those obtained when using all the points of the curve I(V) (Table 5). They confirm that the analysis of the maximum power point's coordinates with the PCA is effective to detect and classify the partial shading (PS) accurately.

The justification for this high classification rate lies in the fact that partial shading more strongly affects the point of maximum power, which is at the inflexion point of the I(V) curve. Therefore, using only this information makes the classification more effective than using all the points of the I(V) curve.



Fig. 10. Projection of the test data in the PCA subspaces

A posteriori class A priori class Class C<sub>0</sub> Class C<sub>1</sub> Class C<sub>2</sub> Class C<sub>3</sub> MPP I(V)MPP I(V)MPP I(V) MPP I(V) Class C<sub>0</sub> 100 97.03 0 0 0 2.97 0 0 Class C<sub>1</sub> 100 99.01 0 0.99 0 0 0 0 Class C<sub>2</sub> 0 0 0 0 100 100 0 0 Class C<sub>3</sub> 0 0 0 100 0 0 0 100

**336** Table 5. Confusion matrix for test data classification

337

338

#### 3.2.4. Robustness of the classification

This section aims to validate the robustness of the fault diagnosis method based on PCA and maximum power point (MPP) coordinates. To do so, previously used faulty MPP data (collected on March 21, 2019), are merged with MPP data collected during healthy operation on June 26, 2018. The corresponding daily profiles of temperature and solar irradiance, as well as the MPP voltage and current evolution under these conditions, are plotted in Fig.11. The robustness is evaluated using the data extracted at different times, and for moderate and high irradiation values. Table 6 presents the new samples used and the ranges of variation of  $T_{PV}$  and  $G_{POA}$ .







Fig. 11. Clear day profiles



Table 6. Extracted samples for robustness evaluation

Samples	Time (h)	T <sub>PV</sub> (°C)	$G_{POA}$ (W/m <sup>2</sup> )
[100;109]	[7h26;7h33]	[36.46 ; 37.9]	[445.53 ; 468.46]
[200;209]	[8h44;8h52]	[48.55 ; 49.81]	[680.71 ; 703.64]
[450;459]	[12h03;12h10]	[63.18;64.19]	[992.10; 1004.50]
[500;509]	[12h43;12h50]	[59.68;62.49]	[967.88;982.80]
[621;630]	[14h22;14h29]	[56.93 ; 58.4]	[797.53;815.39]
[700;709]	[15h29;15h37]	[48.96 ; 50.93]	[606.28;628.28]

349

The new matrix with the merged data  $X_{I40\times3J} = \log[V_{mpp} \quad I_{mpp} \quad P_{mpp}]$  is projected in the PCA 350 subspace spanned by the two principal components (PC1, PC2) obtained in the learning stage with the 351 data collected on March 21, 2019. The results are presented in Fig.12. We observe that class C<sub>0</sub> 352 353 formed with the new healthy measurements is clearly separated from the other three classes of data corresponding to partial shading (PS) conditions. A successful classification of 100% is obtained. 354 Moreover, we notice that all the new test data is positioned between classes C2 and C3, as observed in 355 the previous validation stage. These results are encouraging and prove the robustness of the method 356 357 for PS detection and classification of PV modules.

When looking at the maximum power point's coordinates projected in the PCA subspace, one can 358 observe that classes can be linearly separated. Therefore in the following, linear discriminant analysis 359 (LDA) is used to retrieve the classification laws for fault identification. 360



- 362
- 363



3.3. Features analysis and extraction with Linear Discriminant Analysis (LDA)

#### 3.3.1. Formulation of the LDA algorithm

The LDA algorithm used in [41] [42] [43] will be extended for application to photovoltaic system diagnosis. LDA and PCA share a common characteristic, which is dimension reduction. Nevertheless, theoretically, LDA is more powerful for data classification than PCA because LDA performs dimensionality reduction while keeping maximum the discriminatory information among the classes. For this reason, LDA is generally used to improve data classification when different data classes overlap with the PCA algorithm.

373 Unlike the PCA, the LDA is a supervised analysis technique. It involves a learning phase during which c a priori groups are defined with M descriptive variables and N observations or samples distributed 374 375 into a priori groups, as shown in Figure 13. LDA is both descriptive and decisive. In its descriptive 376 phase, it reduces the size of the data and separates the data according to their a priori defined groups. 377 Linear combinations of the variables in each group create c - l discriminant axes. Each axis is assigned a percentage of the data variance, which is calculated from the corresponding eigenvalue. As in PCA, 378 379 the discriminant axes are ordered in descending order of eigenvalues. In its decisive phase, the LDA 380 generates c - l hyperplanes or separation laws that characterize the differences or similarities between the groups allocated a priori. Thanks to these laws, it is possible to classify new samples of data 381 382 described by the same explanatory variables without a priori knowledge of their group.



Observation *i* for variable  $x_i$ 

383 384

#### Fig. 13. Database organization for LDA algorithm

To perform best linear combinations, LDA aims to obtain a maximum interclass variance which highlights the differences between the classes, and a minimum intraclass variance [44]. The interclass and intraclass variances are respectively estimated by the between matrix variance  $S_B$  and the within matrix variance  $S_w$ .

389 Mathematically formulating, this analysis technique is based on maximizing the following objective390 function, also called Fisher criterion [45]:

391

$$J(u) = \frac{u^T S_B u}{u^T S_w u} \tag{1}$$

392

393 where u is the linear expression that best discriminates all classes of data.

Given *N* observations  $(x_1, x_2, ..., x_N)$  of *M* centered reduced explicative variables,  $N_i$ , the total number of observations for each class  $C_i$ , i = 1, 2, ..., c.

396 Let's consider  $\mu_i$  as the mean value of observations belonging to  $C_i$  and  $\mu$  as the mean value of the 397 entire dataset given by:

$$\mu_i = \frac{1}{N_i} \sum_{x_n \in C_i} x_n \tag{2}$$

$$\mu = \frac{1}{N} \sum_{n=1}^{N} x_n \tag{3}$$

399 The between variance matrix can be expressed as:

$$S_{B} = \sum_{i=1}^{c} (\mu_{i} - \mu)^{T} (\mu_{i} - \mu)$$
(4)

400 The within variance matrix is calculated as:

$$S_w = \sum_{i=1}^c S_i \tag{5}$$

401 where :

402

$$S_{i} = \sum_{x_{n} \in C_{i}} (x_{n} - \mu_{i})^{T} (x_{n} - \mu_{i})$$
(6)

403

404 The eigenvector decomposition of  $S_w^{-1}S_B$  gives the discriminant axes and their corresponding 405 eigenvalues  $\lambda_1, \lambda_2, ..., \lambda_{c-1}$  that indicate the discriminant power of each axis. The eigenvectors 406 associated with the largest eigenvalues define the discriminant axes that span the LDA space for 407 classification. The original data centered reduced are finally projected onto this space to give the data 408 class separability.

- In the decisive phase, LDA uses three quantities to classify the new data samples in one of the defineda priori groups: posterior probability, prior probability, and cost.
- 411 The posterior probability that a new instance or observation *l*, described by the explicative variables, is
- 412 classified into the class  $C_i$  is estimated by the Bayes formula:

$$\hat{P}(C_i/l) = \frac{P(l/C_i).P(C_i)}{P(l)}$$
(7)

413 where  $P(C_i)$  represents the prior probability of class  $C_i$ .

- 414 With this probabilistic approach, the unknown observation l to be identified will be assigned to the
- 415 class  $C_i$  with the highest posterior probability and minimum expected classification cost:

$$\hat{y} = \arg\min_{y=1,..,c} \left( P(C_1 / k)C(y / C_1) + ... + P(C_i / k)C(y / C_i) + ... + P(C_c / k)C(y / C_c) \right)$$
(8)

- 416 Where  $\hat{y}$  is the predicted class, *c* is the number of classes and  $C(y/C_i)$  is the cost of classifying an
- 417 observation as y when its true class is  $C_i$ .
- 418 *3.3.2. Results of the training stage with LDA algorithm*





420

Fig. 14. Fault identification flowchart with LDA algorithm

The flowchart of the proposed algorithm is shown in Fig.14. The LDA is applied to extract the faults discriminating characteristics from maximum power points (MPPs) coordinates. Then, the labels of the data are assigned according to their class of membership (Table 7), and the classifier computes the linear separation laws allowing the classification of new observations. The four a priori classes for original labels are retrieved from the classification results with the PCA algorithm.



Table 7: Fault types and original labels

Condition	Class	Label
Healthy	$C_0$	1

Partial Shading 1	C <sub>1</sub>	2
Partial Shading 2	$C_2$	3
Partial Shading 3	C <sub>3</sub>	4

This training stage is carried out using 67% of the data as original labels. The same matrix 428  $X_{[80\times3]} = \log[V_{mpp} \quad I_{mpp} \quad P_{mpp}]$  built with data recorded on March 21, 2019 is used to extract the fault 429 430 features. Three discriminant axes, also called Fisher axes, are obtained. Fig.15 shows the projection of the training dataset into the 2 - dimensional LDA subspace spanned by the first and the second 431 432 discriminant axes (DA1, DA2). These two axes represent 99.7%, and 0.18% of the data variance, respectively. In this figure, we have also drawn the linear boundaries between the classes. The 433 434 magenta line is the boundary that separates the data for classes C<sub>0</sub> and C<sub>3</sub>. On the other hand, the blue 435 line separates the classes  $C_0$  and  $C_1$ , and the red line separates the observations of  $C_1$  from those of  $C_2$ .

436 Let us consider  $(x_1, x_2)$  as the coordinates of an instance l in the LDA subspace (DA1, DA2). The 437 three boundaries are described by three affine functions  $f_1$ ,  $f_2$  and  $f_3$  where each function  $f_i$  is given by:

438 
$$f_i(x_1, x_2) = L_i(1)x_1 + L_i(2)x_2 + K_i, i = 1, 2, 3$$
(9)

439 The coefficients  $L_i$  and  $K_i$ , i=1, 2, 3, are given in Table 8.





#### 443 **Table 8:** Linear boundaries coefficients

$f_i$	$L_i(1)$	$L_{i}(2)$	<i>K</i> <sub><i>i</i></sub>
$f_1$	$2.93 \ 10^3$	71	$4.7 \ 10^3$
$f_2$	-1.82 104	59	$-2.15\ 10^4$
$f_3$	-1.01 104	17	-1.49 104

444

With the cross-validation method, the same success rate (100%) as for PCA is obtained. LDA also entirely separates the different classes even under climatic variations. In the following, the obtained separation laws will be used to classify new samples; it is the validation stage.

448

#### 449

#### 3.3.3. Results of the validation stage with LDA

The validation is done in two steps. In the first one, the calculated separation laws are used to classify the remaining MPP (test data) representing 33% of the database collected on March 21, 2019. The results, displayed in figure 16 show the successful classification of the test data.

In the second step, the separation laws are evaluated with the healthy samples extracted from measurements on June 26, 2018, mixed with 33% of partial shading data measured on March 21, 2019. The classification result is displayed in Fig.17. With the separation laws, all the test samples are correctly classified in their a priori groups; no misclassification errors were found. With the crossvalidation method, discrimination's effectiveness between the measurements under variable experimental conditions is proved with a success rate of 100 % for all the classes (Table 9).





Fig. 16. Classification of test data in the discrimination space (DA1, DA2)





463

Fig. 17. Classification of mixed data in the discrimination space (DA1, DA2)

# 465

466 Table 9. Confusion matrix for test dataset with LDA

Class	Class a posteriori			
a priori	Class $C_0(\%)$	Class $C_1(\%)$	Class $C_2$ (%)	Class $C_3$ (%)
Class C <sub>0</sub>	100	0	0	0
Class C <sub>1</sub>	0	100	0	0
Class C <sub>2</sub>	0	0	100	0
Class C <sub>3</sub>	0	0	0	100

467

Even if for the studied cases the obtained identification is correct, it can be observed in Fig.17 that healthy state's data corresponding to samples 'test  $C_0$ ', lie on the separation boundary between classes  $C_0$  and  $C_3$ . However, as the probability of assignment to class  $C_0$  is higher, these samples are predicted with label 1 and correctly identified as healthy data. Nevertheless, this ambiguity underlines the fact that in order to have good performance in classifying several types of defects with different levels of severity, it will be beneficial to have a rich database. It must contain several configurations (operating points and states of health) under different environmental conditions.

We can conclude that at the PV module level, the classification of measurements through LDA issuccessful as long as a large amount of labelled data is available for offline learning.



Fault diagnosis based on the analysis of maximum power point's (MPP) coordinates appears to be relevant for large PV plants. Indeed, this approach enables diagnosing a large number of PV modules in real-time faster than using all the points on the I(V) curve, thus reducing power losses and costs.

490 From a field-application perspective, it would be of interest to evaluate these methods with other491 faults.

492 MPP-based methods have up to now only been evaluated at the PV module level. It would be493 interesting to evaluate these methods at the PV string and array levels.

500 498 497 496 494 499 495 [46], [47]. been developed, taking into account the shading condition and have allowed significant energy savings least mitigate series, the shading fault detection and notably the isolation is decisive to balance the modules or at with reconfiguration algorithms to limit the shading effect. When several PV modules are connected in power loss in real-time, thus allowing maintenance optimization. Moreover, they can be combined Besides the ability to PV fault diagnosis, the proposed methods can also be used to quantify the the power production ı gaps between strings. Different reconfigurable architectures have

**Table 10:** Overview of the proposed methods for partial shading detection in PV systems

Pre-processing		Advantages	Limitations for large scale PV plants
•	$\log\left(\frac{\nu}{\eta}\right)$	- Adapted with online I (V) tracer	<ul><li>Less convenient</li><li>Time-consuming and functional</li></ul>
•	log ( <b>i</b> )	- Sensitive to fault severity	disturbance
	$\log(\frac{p}{2})$	- Suitable for small-scale PV	- Power losses
	, η'	systems	<ul> <li>Additionnal cost with local I (V) tracers</li> <li>Sensitive to I (V) curve quality</li> </ul>
•	$\log (I_{MPP})$ $\log (V_{MPP})$ $\log (P_{MPP})$	<ul> <li>allowing an optimized maintenance</li> <li>Cost-effective : no additional measurement of temperature or irradiance for data normalization</li> <li>Saving memory storage</li> <li>Sensitive to fault severity</li> <li>Robust to climatic variations</li> <li>Possible power losses quantification (LDA)</li> </ul>	- Efficient and accurate fault identification depend on the learning data set (size and variety) (LDA)

Variables	<ul> <li>Current <i>i</i></li> <li>Voltage <i>v</i></li> <li>Power <i>p</i></li> <li>303 observations for each variable</li> </ul>	<ul> <li>Current <i>I<sub>MPP</sub></i></li> <li>Voltage <i>V<sub>MPP</sub></i></li> <li>Power <i>P<sub>MPP</sub></i></li> <li>Bo observations for each variable</li> </ul>
Method	<ul> <li>I (V) curve analysis –</li> <li>PCA [22]</li> </ul>	<ul> <li>MPP</li> <li>analysis -</li> <li>PCA</li> <li>MPP</li> <li>analysis -</li> <li>LDA</li> </ul>

502

#### 5. Conclusion

503 504

Fault detection and identification in PV systems are essential to expedite the maintenance and 505 506 minimize the power losses. This study has presented a cost-effective and straightforward data-driven 507 diagnosis approach to detect and identify partial shading using principal component analysis (PCA) 508 and linear discriminant analysis (LDA). No prior information on the PV system and no other sensing circuit are needed. The proposed methods take advantage of available measurements in PV systems: 509 510 voltage, current, and power at the maximum power point (MPP). The effectiveness of the proposed methods has been successfully proved at the PV module level. Based on collected data under real 511 512 working conditions (variable irradiation and temperature), we have demonstrated that the methods can 513 correctly detect and classify the partial shading fault with a success rate of 100%. The methods are 514 also easy to integrate into a monitoring system for real-time diagnosis and are especially convenient 515 for large-scale PV plants. The data required for the learning stage can benefit from the vast amount of data available in PV plants under operation for decades. Otherwise, the learning database could be 516

- 517 generated from simulation models. It would be of interest to evaluate the proposed methodology with
- 518 other faults (open-circuit, short-circuit, and contact degradation).

### 520 Acknowledgement

The authors gratefully recognize the financial support of the Ministry of Higher Education and
 Scientific Research in Tunisia and Paris-Saclay University who provided the scholarship to the PhD
 student.

524

# 525 **References**

- A. Golnas, "PV System Reliability: An Operator's Perspective," *IEEE J. Photovolt*, vol. 3, no. 1,
   pp. 416–421, 2013, doi: 10.1109/JPHOTOV.2012.2215015.
- 528 [2] ÎÊA, "Reliability Study of Grid Connected PV Systems," T7-08, 2002.
- Y. Zhao, R. Ball, J. Mosesian, J. de Palma, and B. Lehman, "Graph-Based Semi-supervised Learning for Fault Detection and Classification in Solar Photovoltaic Arrays," *IEEE Trans. Power Electron*, vol. 30, no. 5, pp. 2848–2858, 2015, doi: 10.1109/TPEL.2014.2364203.
- 532 [4] D. C. Jordan, T. J. Silverman, J. H. Wohlgmuth, S. R. Kurtz, and K. T. VanSant, "Photovoltaic failure and degradation modes," *Prog. Photovolt: Res. Appl.*, pp. 318–326, 2017, doi: 10.1002/pip.2866.
- 535 [5] IEA, "Assessment of Photovoltaic Module Failures in the Field," 2017.
- 536 [6] X. Sun, R. V. K. Chavali, and M. A. Alam, "Real-time monitoring and diagnosis of photovoltaic
  537 system degradation only using maximum power point—the Suns-Vmp method," *Prog Photovolt*538 *Res Appl*, vol. 27, no. 1, pp. 55–66, 2019, doi: 10.1002/pip.3043.
- M. Bressan, Y. El Basri, A. G. Galeano, and C. Alonso, "A shadow fault detection method based on the standard error analysis of I-V curves," *Renew.Energy*, vol. 99, pp. 1181–1190, 2016, doi: 10.1016/j.renene.2016.08.028.
- 542 [8] A. Y. Appiah, X. Zhang, K. A. Ben Beklisi, and F. Kyeremeh, "Review and performance evaluation of photovoltaic array fault detection and diagnosis techniques," *Int. J. Photoenergy*, vol. 2019, pp. 1–19, 2019, doi: https://doi.org/10.1155/2019/6953530.
- A. Triki-Lahiani, A. Bennani-Ben Abdelghani, and I. Slama-Belkhodja, "Fault detection and monitoring systems for photovoltaic installations: A review," *Renew. Sustain. Energy Rev*, vol. 82, pp. 2680–2692, 2018, doi: https://doi.org/10.1016/j.rser.2017.09.101.
- 548 [10] D. S.Pillai, F. Blaabjerg, and N. Rajasekar, "A comparative Evaluation of Advanced Fault
  549 Detection Approaches for PV Systems," *IEEE Journal of Photovoltaics*, vol. 9, no. 2, pp. 513–
  550 527, 2019, doi: 10.1109/JPHOTOV.2019.2892189.
- [11] S. Daliento *et al.*, "Monitoring, Diagnosis, and Power Forecasting for Photovoltaic Fields: A
  Review," *International Journal of Photoenergy*, pp. 1–13, 2017, doi: https://doi.org/10.1155/2017/1356851.
- 554 [12] F. Spertino *et al.*, "A power and energy procedure in operating photovoltaic systems to quantify
  555 the losses according to the causes," *Sol.Energy*, vol. 118, pp. 313–326, 2015, doi:
  556 https://doi.org/10.1016/j.solener.2015.05.033.
- [13] IEA, "Review on Infrared and Electroluminescence Imaging for PV Field Applications," T13 10, 2018.

- 559 [14] M. Wolfgang, C. Hirschl, L. Neumaier, A. Kolger, and A. Plosch, "Identifikation von fehlerhaften PV Modulen und Anlangen mit Thermografie," presented at the 29. Symposium 560 Photovoltaische Solarenergie 2014, Deutschland, 2014, pp. 1–11, doi: 10.13140/2.1.3636.2881. 561
- [15] J. A. Tsanakas, L. D. Ha, and F. AL Shakarchi, "Advanced inspection of photovoltaic 562 563 installations by aerial triangulation and terrestrial georeferencing of thermal/visual imagery," Renew.Energy, vol. 102, pp. 224–233, 2017, doi: https://doi.org/10.1016/j.renene.2016.10.046. 564
- [16] S. Roy, M. K. Alam, F. Khan, J. Johnson, and J. Flicker, "An Irradiance-Independent, Robust 565 566 Ground-FaultDetection Scheme for PV Arrays Based on SpreadSpectrum Time-Domain Reflectometry (SSTDR)," IEEE Trans. Power Electron, vol. 33, no. 8, pp. 7046–7057, 2018, 567 doi: 10.1109/TPEL.2017.2755592. 568
- [17] M. K. Alam, F. Khan, J. Johnson, and J. Flicker, "PV ground-fault detection using spread 569 570 spectrum time domain reflectometry (SSTDR)," presented at the IEEE Energy Conversion 571 Congress and Exposition (ECCE), USA, 2013, pp. 1015–1020, doi: 572 10.1109/ECCE.2014.6953848.
- [18] M. K. Alam, F. Khan, J. Johnson, and J. Flicker, "PV arc-fault detection using spread spectrum 573 574 time domain reflectometry (SSTDR)," presented at the IEEE Energy Conversion Congress and 575 Exposition (ECCE), USA, 2014, pp. 3294-3300, doi: 10.1109/ECCE.2014.6953848.
- [19] T. Takashima, J. Yamaguchi, and M. Ishida, "Fault detection by signal response in PV module 576 strings," presented at the 33rd IEEE Photovoltaic Specialists Conference, USA, 2008, doi: Fault 577 detection by signal response in PV module strings. 578
- 579 [20] T. Takashima, J. Yamaguchi, K. Otani, T. Oozeki, K. Kato, and M. Ishida, "Experimental studies of fault location in PV module strings," Sol. Energy Mater. and Sol. Cells, vol. 93, no. 6-580 7, pp. 1079–1082, 2009, doi: https://doi.org/10.1016/j.solmat.2008.11.060. 581
- 582 [21] S. Fadhel, A. Migan, C. Delpha, D. Diallo, I. Bahri, M. Trabelsi, M.F. Mimouni, "Data-driven Approach for Isolated PV Shading Fault Diagnosis Based on Experimental I-V curves Analysis," 583 584 presented at the IEEE International Conference on Industrial Technology (ICIT), France, 2018, pp. 927-932, doi: 10.1109/ICIT.2018.8352302. 585
- [22] S. Fadhel, C. Delpha, D. Diallo, I. Bahri, A. Migan, M. Trabelsi, M.F. Mimouni, "PV shading 586 587 fault detection and classification based on I-V curve using principal component analysis: 588 Application to isolated PV system," Sol.Energy, vol. 179, pp. 1-10, 2019.
- [23] Y. El Basri, M. Bressan, L. Seguir, H. Alawadhi, and C. Alonso, "A proposed graphical 589 590 electrical signatures supervision method to study PV module failures," Sol. Energy, vol. 116, pp. 591 247-256, 2015, doi: https://doi.org/10.1016/j.solener.2015.02.048.
- 592 [24] A. K. Tossa, Y. M. Soro, Y. Azoumah, and D. Yamegueu, "A new approach to estimate the 593 performance and energy productivity of photovoltaic modules in real operating conditions," Sol.Energy, vol. 110, pp. 543–560, 2014, doi: 10.1016/j.solener.2014.09.043. 594
- [25] M. Merchaoui, A. Sakly, and M. F. Mimouni, "Particle swarm optimisation with adaptive 595 596 mutation strategy for photovoltaic solar cell/module parameter extraction," Energy Conv. and Manag, vol. 175, pp. 151–163, 2018, doi: https://doi.org/10.1016/j.enconman.2018.08.081. 597
- 598 [26] Y. Chaibi, M. Malvoni, A. Chouder, M. Boussetta, and M. Salhi, "Simple and efficient approach to detect and diagnose electrical faults and partial shading in photovoltaic systems," *Energy* 599 Conversion and Management, vol. 196, pp. 330-343, 2019, doi: 600
- https://doi.org/10.1016/j.enconman.2019.05.086. 601
- [27] D. S.Pillai and N. Rajasekar, "Metaheuristic algorithms for PV parameter identification: A 602 603 comprehensive review with an application to threshold setting for fault detection in PV systems," Renew. Sustain. Energy Rev, vol. 82, pp. 3503–3525, 2018, doi: 604 https://doi.org/10.1016/j.rser.2017.10.107 Get. 605
- 606 [28] S. Kichou, S. Silvestre, L. Guglielminotti, L. Mora-Lopez, and E. Munoz-Ceron, "Comparison of two PV array models for the simulation of PV systems using five different algorithms for the 607

- parameters identification," *Renew.Energy*, vol. 99, pp. 270–279, 2016, doi:
   https://doi.org/10.1016/j.renene.2016.07.002.
- [29] Z. Chen, L. Wu, S. Cheng, P. Lin, W. Yue, and W. Lin, "Intelligent fault diagnosis of
  photovoltaic arrays based on optimized kernel extreme learning machine and I-V
  characteristics," *Applied Energy*, vol. 204, pp. 912–931, 2017, doi:
  https://doi.org/10.1016/j.apenergy.2017.05.034.
- [30] S. Spataru, D. Sera, T. Kerekes, and R. Teodorescu, "Diagnostic method for photovoltaic
  systems based on light I–V measurements," *Sol.Energy*, vol. 119, pp. 29–44, 2015, doi:
  10.1016/j.solener.2015.06.020.
- [31] J. D. Bastidas-Rodr´ıguez, E. Franco, G. Petrone, C. A. Ramos-Paja, and G. Spagnuolo, "Model
  Based Degradation Analysis Of Photovoltaic Modules Through Series Resistance Estimation," *IEEE Trans. Indus. Electr.*, vol. 62, no. 11, pp. 7256–7265, 2015, doi:
  10.1109/TIE.2015.2459380.
- [32] D. Wang, "A method for instantaneous measurement of PV I-V characteristics and its
  application for MPPT control," presented at the 35th IEEE Photovoltaic Specialists Conference,
  USA, 2010, pp. 2904–2907, doi: 10.1109/PVSC.2010.5614505.
- [33] A. Khoshnami and I. Sadeghkhani, "Sample entropy-based fault detection for photovoltaic
  arrays," *IET Renew. Power Gener*, vol. 12, no. 16, pp. 1966–1976, 2018, doi: 10.1049/ietrpg.2018.5220.
- [34] M. Dhimish, V. Holmes, B. Mehrdadi, and M. Dales, "Multi-layer photovoltaic fault detection algorithm," *IET High Voltage*, vol. 4, pp. 244–252, 2017, doi: 10.1049/hve.2017.0044.
- [35] F. Harrou, A. Dairi, B. Taghezouit, and Y. Sun, "An unsupervised monitoring procedure for detecting anomalies in photovoltaic systems using a one-class Support Vector Machine," *Sol.Energy*, vol. 179, pp. 48–58, 2019, doi: https://doi.org/10.1016/j.solener.2018.12.045.
- [36] E. Garoudja, F. Harrou, Y. Sun, K. Kara, A. Chouder, and S. Silvestre, "Statistical fault detection in photovoltaic systems," *Sol.Energy*, vol. 150, pp. 485–499, 2017, doi: https://doi.org/10.1016/j.solener.2017.04.043.
- [37] L. Garcia-Gutierrez, M. Bressan, F. Jimenez, S. de-las Heras, and C. Alonso, "Design of a
  Global Maximum Power Point Tracking (GMPPT) for PV array based on precise PV shadow
  model," presented at the 7th International Conference on Renewable Energy Resarch and
  Applications (ICRERA), Paris, France, Oct. 2018, pp. 275–280, doi:
  10.1109/ICRERA.2018.8566880.
- [38] M. Aquib, S. Jain, and V. Agarwal, "A Time-Based Global Maximum Power Point Tracking
  Technique for PV System," *IEEE Trans. Power Electr.*, vol. 35, no. 1, pp. 393–402, 2020, doi:
  10.1109/TPEL.2019.2915774.
- [39] K. Kobayashi, I. Takano, and Y. Sawada, "A study of a two stage maximum power point tracking control of a photovoltaic system under partially shaded insolation conditions," *Sol. Energy Mater. and Sol. Cells*, vol. 90, pp. 2975–2988, 2006, doi: https://doi.org/10.1016/j.solmat.2006.06.050.
- [40] H. Zhu, L. Lu, J. Yao, S. Dai, and Y. Hu, "Fault diagnosis approach for photovoltaic arrays
  based on unsupervised sample clustering and probabilistic neural network model," *Sol.Energy*,
  vol. 176, pp. 395–405, 2018, doi: https://doi.org/10.1016/j.solener.2018.10.054.
- [41] M. Benbouzid, C. Delpha, Z. Khatir, S. Lefebvre, and D. Diallo, "Faults Detection and
  Diagnosis in a Static Converter," in *Electrical Machine Diagnosis*, ISTE., 2011, pp. 272–319.
- [42] D. Y. Jung, S. M. Lee, H. Wang, J. H. Kim, and S. H. Lee, "Fault detection method with PCA and LDA and its application to induction motor," *J. Cent. South Univ. Technol.*, vol. 17, pp. 1238–1242, 2010, doi: https://doi.org/10.1007/s11771-010-0625-y.
- [43] R. J. Martis, U. R. Acharya, and L. C. Min, "ECG beat classification using PCA, LDA, ICA and
  Discrete Wavelet Transform," *Biomedical Signal Processing and Control*, vol. 8, pp. 437–448,
  2013, doi: https://doi.org/10.1016/j.bspc.2013.01.005.

- 658 [44] A. Quinquis, *Digital Signal Processing using MATLAB*, ISTE. André Quinquis, 2008.
- [45] K. V. Mardia, J. T. Kent, and J. M. Bibby, *Multivariate Analysis*. New York, 1979.
- [46] M. A. Chaaban *et al.*, "Adaptive photovoltaic system," presented at the 36th Annual Conference
  on IEEE Industrial Electronics Society (IECON), USA, 2010, pp. 3192–3197, doi:
  10.1109/IECON.2010.5675047.
- [47] M. Alahmad, M. A. Chaaban, S. kit Lau, J. Shi, and J. Neal, "An adaptive utility interactive
   photovoltaic system based on a flexible switch matrix to optimize performance in real-time,"
- 665 *Sol.Energy*, vol. 86, pp. 951–963, 2012, doi: https://doi.org/10.1016/j.solener.2011.12.028.
- 666