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# Transient analysis of solar pyrolysis and hydrogen yield via interband cascade laser absorption spectroscopy of methane, acetylene, ethylene, and ethane

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## ABSTRACT

A mid-infrared laser absorption sensing method has been developed to measure species concentrations of four hydrocarbons and gas temperature over a range of temperatures in mixture compositions relevant to the pyrolytic decomposition of natural gas. The four measured species (methane, acetylene, ethylene, and ethane) are the most abundant hydrocarbons during the pyrolysis of natural gas, and provide a means to monitor decomposition progress and hydrogen yield through molar balance. In this work, time-division multiplexed signals of three distributed-feedback interband cascade lasers are used to make simultaneous measurements of select C-H stretch rovibrational transitions of the target hydrocarbons in the 3.00–3.34 μm range. The sensor was validated over a range of temperatures and pressures (300–1000 K, 0.03–1 atm) at relevant mixture compositions, with correction methods developed to mitigate cross-species interference. The sensor was demonstrated on a solar-thermal pyrolysis reactor, where time-resolved measurements of species mole fractions were performed across a range of insolation conditions to capture the transient response of the reactor.

## 1. Introduction

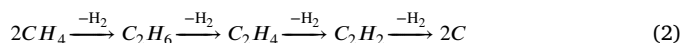
Hydrogen (H<sub>2</sub>) is considered to be an important alternative to traditional hydrocarbon fuels for the purpose of decreasing global anthropogenic carbon dioxide (CO<sub>2</sub>) emissions [1]. Currently, approximately 96% of H<sub>2</sub> is produced via thermochemical conversion of carbon-based fuels [2]. Of these thermochemical processes, the leading method for hydrogen production is steam-methane reforming (SMR) [3]. In this endothermic reaction, high temperature steam reacts with methane (CH<sub>4</sub>) gas to produce H<sub>2</sub> amongst byproducts that include CO<sub>2</sub>. The heat source for this reaction is primarily derived from the use of fossil fuels, further increasing the net CO<sub>2</sub> emissions [4]. CH<sub>4</sub> pyrolysis offers an alternative to SMR for hydrogen production with less CO<sub>2</sub> emissions [5]. The global chemical equation for this reaction is given by:



Like SMR, the pyrolysis of CH<sub>4</sub> is also an endothermic reaction. However, the absence of any oxidizer in the reactants precludes the formation of CO<sub>2</sub> in the products. In addition, the pure solid carbon products formed through the pyrolytic reaction are more readily separated from

the gaseous product stream and sold or stored at a favorable economical value compared to gaseous oxidized carbon [6]. Here, we report detailed optical diagnostics of the gaseous product stream in a methane pyrolysis reaction driven by solar-thermal stimulus.

As shown below, the pyrolytic decomposition of CH<sub>4</sub> generally progresses in a stepwise dehydrogenation, where the successive loss of H<sub>2</sub> molecules corresponds with the formation of stable intermediates with increased C:H ratio [7].



The CH<sub>4</sub> decomposition process is simulated using a more comprehensive reaction mechanism (USC Mech II) at a constant temperature of 1400 K in Fig. 1, showing that methane, acetylene (C<sub>2</sub>H<sub>2</sub>), ethylene (C<sub>2</sub>H<sub>4</sub>), and ethane (C<sub>2</sub>H<sub>6</sub>) represent the dominant gas-phase intermediate and product constituents [8]. As such, quantitative measurements of these four hydrocarbons in the product stream provide critical information about reaction progress as well as process efficiency. Although the present work focuses on methane pyrolysis, it is important to note that other, larger hydrocarbon feedstocks (alkane, alkene,

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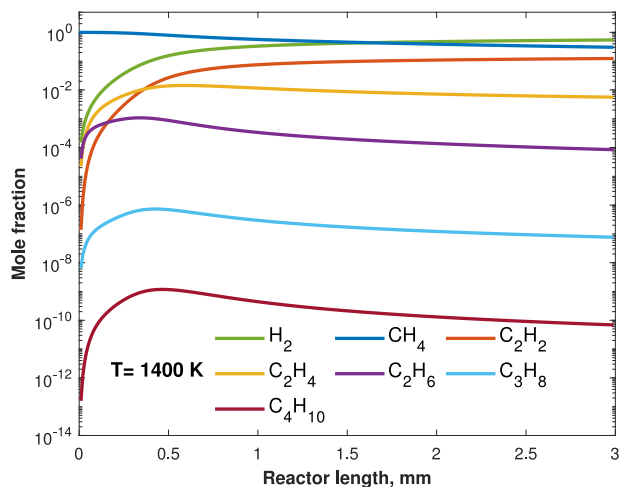


Fig. 1. Species evolutions obtained from a chemical kinetic simulation of  $\text{CH}_4$  decomposition through a plug flow reactor at 25 torr and a gas flow rate of 100 sccm using CANTERA [22]. Relevant reactions were obtained from the USC Mech II chemical mechanism [8].

and alkyne) similarly decompose into these intermediates which represent the smallest stable species of various carbon-hydrogen bond structures [9].

This work focuses on  $\text{CH}_4$  pyrolysis due to the abundance of  $\text{CH}_4$  in natural gas, the most common feedstock in  $\text{H}_2$  production. In this context, it can be shown that measurement of the target hydrocarbon species can well-characterize the gas-phase output with hydrogen being the only remaining species of significant concentration. Time-resolved species measurements may further be used in process development or control, where a snapshot of reaction progress or process efficacy can then inform changes to operational parameters to improve yield quality.

$\text{CH}_4$  pyrolysis has been studied through a multitude of reactor configurations (fixed bed, fluidized bed, plasma-assisted) and through catalyzed or uncatalyzed processes [10–12]. Typically, the product stream for such systems is characterized ex-situ via either mass spectrometry (MS) or gas chromatography (GC). The inherent response times of these sample-based monitoring techniques (on the order of seconds to minutes) are often adequate for final product compositional analysis. However, in order to elucidate transient decomposition behavior and to optimize process conditions in real time, particularly under variable heating, faster response times are desired. In addition, the quantification of trace species such as  $\text{C}_2\text{H}_4$  and  $\text{C}_2\text{H}_6$  requires high sensitivity, often outside the detection range of more portable and affordable MS and GC devices [13]. GC-MS also typically requires calibration to be quantitative, which can be challenging in complex gas mixtures.

By contrast, laser absorption spectroscopy (LAS) provides a highly quantitative, calibration-free, and in-situ or in-stream method for measuring both dominant and trace hydrocarbon species formed in the pyrolytic decomposition of  $\text{CH}_4$  based on molecular structure rather than mass or chemical interactions. LAS sensing of  $\text{CH}_4$ ,  $\text{C}_2\text{H}_2$ ,  $\text{C}_2\text{H}_4$ , and  $\text{C}_2\text{H}_6$  has been demonstrated across a variety of applications. These applications include environmental monitoring [14,15], combustion chemistry studies [16–18] and planetary sciences [19] as well. The recent emergence of distributed-feedback interband cascade lasers (DFB-ICLs) has enabled highly sensitive detection of these C1-C2 hydrocarbons in the C-H stretch fundamental bands [20,21], providing enhanced detection limits and in situ measurements over short optical pathlengths.

In a recent study by our research group, Wei et al. [23] employed an LAS measurement technique to characterize the product stream in

a solar-thermal pyrolysis reactor. In that work, two DFB-ICLs were deployed to measure  $\text{CH}_4$ ,  $\text{C}_2\text{H}_4$ , and  $\text{C}_2\text{H}_6$  at the exhaust of a solar reactor through regularly-intervalled diversion of the beams on the order of Hz. The method was used to make species measurements over a range of pyrolysis conditions, and provided important benchmark data for comparison to first-order chemical kinetic models of the reactor [23].

The present work advances upon this prior LAS sensor development via several key elements: (1) addition and integration of a  $\text{C}_2\text{H}_2$  measurement strategy to further understanding of the latter dehydrogenation steps and to improve estimation of hydrogen yield, (2) simultaneous kHz-rate sensing of the four hydrocarbon species via time-division-multiplexing on a shared beam path, and (3) extension of the thermodynamic range of the multi-species LAS method to elevated temperatures with validated correction methods to mitigate the effects of cross-species interference. In this paper, we present the theory and methods underlying this novel laser diagnostic strategy for time-resolved measurement of species yields in hydrocarbon pyrolysis. Sensor capabilities are tested via a series of validation tests and a demonstration for transient analysis of a solar-thermal pyrolysis reactor.

## 2. Laser absorption spectroscopy (LAS)

### 2.1. Theory

The theory of LAS is extensively outlined in prior work [24] and is only briefly discussed here to clarify nomenclature. Thermodynamic gas properties and species mole fraction,  $X_{abs}$ , are related to the transmitted intensity of monochromatic light by the Beer–Lambert law given by:

$$\alpha_\nu = -\ln\left(\frac{I_\nu}{I_0}\right)_\nu = \sum_i P x_{abs} S_i(T) \varphi_i(\nu, T, P, X_{abs}) L \quad (3)$$

where  $I_\nu/I_0$  is the ratio of experimentally measured transmitted and incident laser intensity at frequency  $\nu$  [ $\text{cm}^{-1}$ ],  $\alpha_\nu$  is the spectral absorbance at that frequency,  $P$  [atm] is the total pressure,  $S_i(T)$  [ $\text{cm}^{-2}/\text{atm}$ ] is the temperature-dependent linestrength of transition  $i$  at temperature  $T$  [K],  $L$  [cm] is the pathlength of the absorbing medium, and  $\varphi_i$  [cm] is the spectral lineshape of transition  $i$ . Integrating over the spectral domain of a well-isolated transition yields the absorbance area,  $A_i$ :

$$A_i = \int_{-\infty}^{\infty} \alpha_\nu d\nu = P S_i(T) x_{abs} L \quad (4)$$

This integration eliminates the lineshape dependence on the absorbance area. In practice, this is achieved by fitting an assumed lineshape to the measured spectra. With independent knowledge of pressure, temperature, and the pathlength of the absorbing gas, the species mole fraction may be determined.

In addition, the availability of two sufficiently-isolated transitions of a given species allows for a gas temperature measurement through a two-line thermometry technique. By taking a ratio of the absorbance areas of these transitions, the dependence on pressure, species mole fraction, and pathlength is eliminated. As a result, the ratio of areas shown in Eq. (5) is only dependent on temperature, as below:

$$\frac{A_i}{A_j} = \frac{S_i(T)}{S_j(T)} \quad (5)$$

Eq. (5) can then be solved to obtain the temperature of a given gas.

## 2.2. Wavelength selection

Recent advances in laser technology have made the strongest mid-wave infrared (IR) vibrational bands of hydrocarbons readily-accessible for tunable laser absorption spectroscopy. The line survey in Fig. 2 shows several vibrational bands of the target hydrocarbons (methane, acetylene, ethylene, and ethane) in the infrared, including the fundamental C-H stretch vibrational bands in mid-IR (3–4  $\mu\text{m}$ ). These fundamental bands are orders of magnitude stronger than the overtone and combination bands found in the near-IR. In this work, interband cascade lasers are used to probe these strong mid-IR transitions, and facilitate sensitive measurement of hydrocarbons formed in pyrolytic reactions.

Select rovibrational transitions from the C-H stretch bands in the 3.00–3.34  $\mu\text{m}$  range (indicated by the dashed lines in the line survey and the absorbance subplot in Fig. 2) were chosen to probe each hydrocarbon. The R(15) manifold of the  $\nu_3$  band of  $\text{CH}_4$  was selected for measurements near room temperature due to its relative strength and isolation from other hydrocarbon transitions [25]. The strong absorption linestrength enables a wide dynamic range of  $X_{\text{CH}_4}$  measurements, a critical requirement for characterizing the efficacy of pyrolytic reactors that use either  $\text{CH}_4$  or natural gas as a feed gas. However, at elevated temperatures ( $T > 479$  K), this R(15) manifold can become optically thick at moderate pathlengths ( $\sim 10$  cm), thus preventing accurate inference of  $X_{\text{CH}_4}$ . To avert this issue and extend the range of operation, a separate wavelength region consisting of multiple transitions adjacent to the R(15) manifold was instead used for  $X_{\text{CH}_4}$  determination. These two separate wavelength regions are shown in the middle inset of the spectral simulation subplot in Fig. 2, also highlighting the R(14) transition of the  $\nu_9$  band of  $\text{C}_2\text{H}_4$  that was probed in this work. This  $\text{C}_2\text{H}_4$  transition was selected primarily for its proximity to the R(15) manifold of  $\text{CH}_4$  [23], enabling simultaneous measurement of the two species using one laser. Acetylene is commonly the second most abundant product species during the pyrolysis of  $\text{CH}_4$  or natural gas, and was probed here by measurement of the adjacent R(24) and R(18) line pair of the  $\nu_2 + \nu_4 + \nu_5$  and  $\nu_3$  bands, respectively [26]. These transitions were selected for their strong absorption linestrengths and relative isolation from the transitions of other hydrocarbons, enabling determination of  $X_{\text{C}_2\text{H}_2}$  without any necessary interference-mitigating correction methods. The trace amount of  $\text{C}_2\text{H}_6$  formed in the aforementioned pyrolytic reactions was measured by targeting the intense  $^{\text{R}}\text{Q}_3$  line cluster near 2996.86  $\text{cm}^{-1}$ , selected for strength and relative isolation [27]. The management of cross-species interference at this wavelength at certain conditions is further detailed in the sensor validation and data processing section.

## 2.3. Optical setup

Three distributed feedback interband cascade lasers were used in this work to target the four hydrocarbons in a time-division-multiplexed optical configuration (see Fig. 3). Colinear propagation and delivery of the three beams from the breadboard were achieved using two carefully-aligned  $\text{CaF}_2$  beam splitters. Time-multiplexed trapezoidal waveforms of varying effective duty cycle (20%–30%) was selected for modulation as it maximized the output laser beam power during the scan period while minimizing any ringing effects and also allowing all three lasers to scan during a single period, providing a raw measurement rate of 10 kHz [31]. The colinear, time-multiplexed laser beams were transmitted through sapphire windows and focused onto a single photovoltaic (PV) detector (VIGO System PVI-4TE-5, 100 MHz bandwidth). A 2-inch germanium etalon with a free spectral range of 0.024  $\text{cm}^{-1}$  was placed along the beam path to convert light intensity signals from the time domain to the wavenumber domain. These etalon signals were recorded for each laser prior to each test. All signals were recorded using a 200-MHz bandwidth oscilloscope (Picoscope 5000 series). A raw sample signal of the simultaneous measurement of the

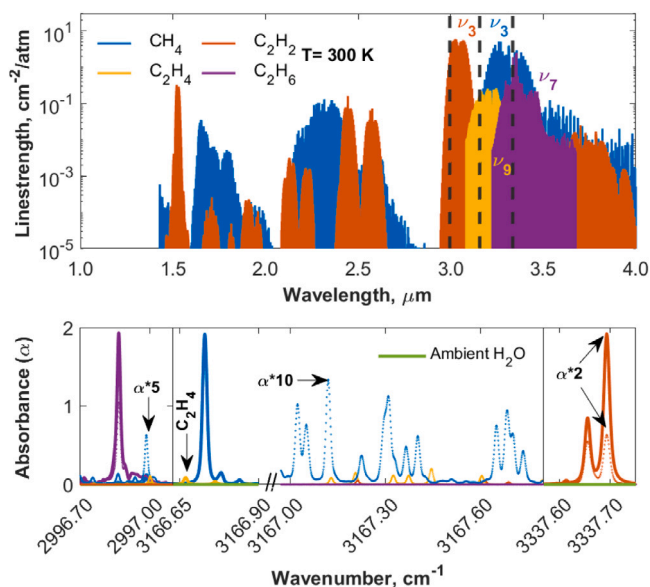


Fig. 2. (Top) Absorption linestrengths of hydrocarbons relevant to this study computed from the HITEMP [28] database ( $\text{CH}_4$ ), HITRAN [29] database ( $\text{C}_2\text{H}_2$  and  $\text{C}_2\text{H}_4$ ) and cross-sectional database by Harrison et al. [30] ( $\text{C}_2\text{H}_6$ ). Dashed lines indicate the specific wavenumbers used. (Bottom) Spectral simulations of the measured transitions and interfering partners at  $P = 45$  torr,  $L = 10$  cm, and mole fractions: 92%  $\text{CH}_4$ , 4%  $\text{C}_2\text{H}_2$ , 3%  $\text{C}_2\text{H}_4$  and 1%  $\text{C}_2\text{H}_6$  at  $T = 300$  K (solid lines) and at  $T = 600$  K (dashed lines). Simulations of  $\text{H}_2\text{O}$  are included to account for potential ambient absorption in the beam path of the lasers.

spectra of the four hydrocarbons is shown in Fig. 4. A phase-locked average was often employed to improve signal to noise ratio (SNR) and detection at trace levels and yielded an effective time resolution of 1 ms, more than adequate for process monitoring. In addition to facilitating the simultaneous measurement of the hydrocarbon species, this optical configuration and time-multiplexing scheme removed the need for active physical diversion of the individual beams through the use of a flip mirror as employed by Wei et al. [23], which had been cumbersome and significantly limited overall measurement rate. This compact, modular configuration allowed for the seamless integration of the LAS sensor module with both the solar-thermal reactor and the high-temperature gas cell that was used for validation measurements.

## 3. Sensor validation

In this section, the species-specific spectroscopic methods employed to make quantitative inferences of individual species mole fractions are detailed. For these validation measurements, the LAS sensor module described in the previous section was aligned on an optically-accessible heated gas cell [32] as illustrated in Fig. 3. Measurements presented in this section were made using a gas mixture with the following nominal composition: 92.05%  $\text{CH}_4$ , 4%  $\text{C}_2\text{H}_2$ , 3%  $\text{C}_2\text{H}_4$ , and 0.95%  $\text{C}_2\text{H}_6$ . This specific composition was selected to enable the investigation of spectral interference and demonstrate the sensor capability to perform species measurements at a relevant composition to the pyrolysis of natural gas and methane, which is the primary target application.

### 3.1. Data processing & fitting procedures

Measured absorbance spectra were least-squares fitted with Voigt lineshapes, and quantitative inference of species abundance was achieved using spectral parameters from HITEMP ( $\text{CH}_4$ ), HITRAN ( $\text{C}_2\text{H}_2$  and  $\text{C}_2\text{H}_4$ ) and the cross-sectional database by Harrison et al. ( $\text{C}_2\text{H}_6$ ). The Doppler linewidth for all lines was calculated using an average temperature measured from three thermocouples equally spaced along the length of the gas cell. The static pressure of the gas was measured using capacitance manometers.

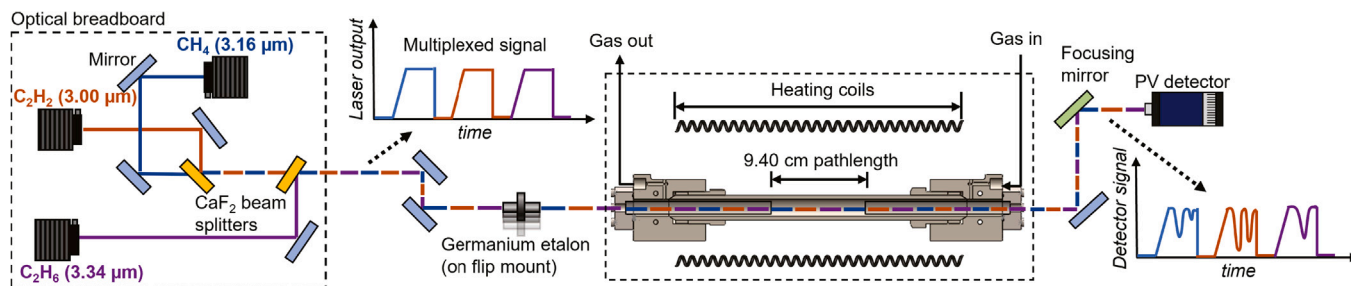


Fig. 3. Schematic illustrating the LAS sensor module (left) interfaced with the high-temperature gas cell (right).

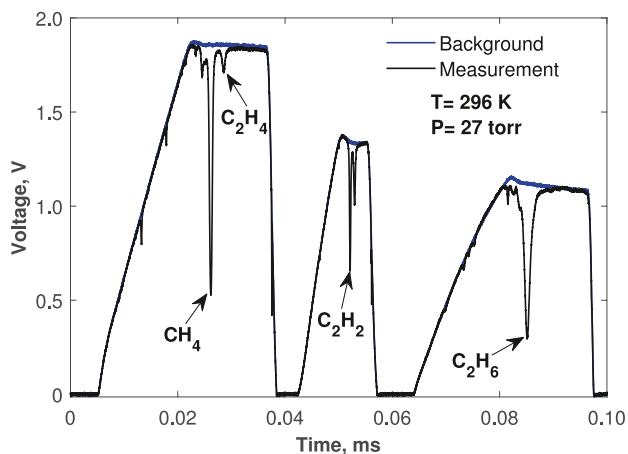


Fig. 4. Time-division multiplexed raw signals illustrating the simultaneous measurement of the spectra of all four hydrocarbons in a gas cell with an optical pathlength of 9.4 cm. The species mole fractions are: 92.05%  $\text{CH}_4$ , 4%  $\text{C}_2\text{H}_2$ , 3%  $\text{C}_2\text{H}_4$  and 0.95%  $\text{C}_2\text{H}_6$ .

### 3.1.1. $\text{C}_2\text{H}_2$ spectral fitting and thermometry

The spectral region at which the  $\text{C}_2\text{H}_2$  measurement was made is free of interference from other measured hydrocarbons. This allows for direct spectral fitting of the measurement without need for interference-correction. The two  $\text{C}_2\text{H}_2$  transitions were least-squares fitted using Voigt profiles with the absorbance areas,  $A_i$  and collisional linewidths,  $\nu_c$  treated as free parameters directly. The mole fraction,  $X_{\text{C}_2\text{H}_2}$ , was then recovered from both these fitted absorbance areas through the application of Eq. (4). The availability of two closely-spaced transitions in the  $\text{C}_2\text{H}_2$  measurement domain with differing lower state energy enabled the radiometric inference of the gas temperature as well. Using the measured absorbance area of each transition to obtain an area ratio, Eq. (5) was solved iteratively to obtain temperature. As shown in Fig. 5, this temperature measurement technique demonstrated good accuracy up to  $\sim 800$  K, with a standard deviation of  $\sim 3\%$  from known thermocouple measurements. At temperatures higher than 805 K, the inferred temperature showed significant deviation from thermocouple measurements. This is attributed to the inability of the HITRAN database to fully capture the spectra at these high temperatures (due to additional high rotational energy lines not in HITRAN becoming active) and the relatively low lower-state energy difference of the line pair of  $303 \text{ cm}^{-1}$ .

### 3.1.2. Sequential fitting of $\text{CH}_4$ and $\text{C}_2\text{H}_4$ spectra

Due to the large disparity in the respective peak absorbance of the target  $\text{C}_2\text{H}_4$  and  $\text{CH}_4$  transitions highlighted in Fig. 6, a simultaneous fit of the two transitions yielded unreliable results, with the fitting routine exhibiting a bias towards the much stronger  $\text{CH}_4$  transition. To address this issue, a sequential fitting routine of the two species' transitions was employed as it yielded more accurate determination of

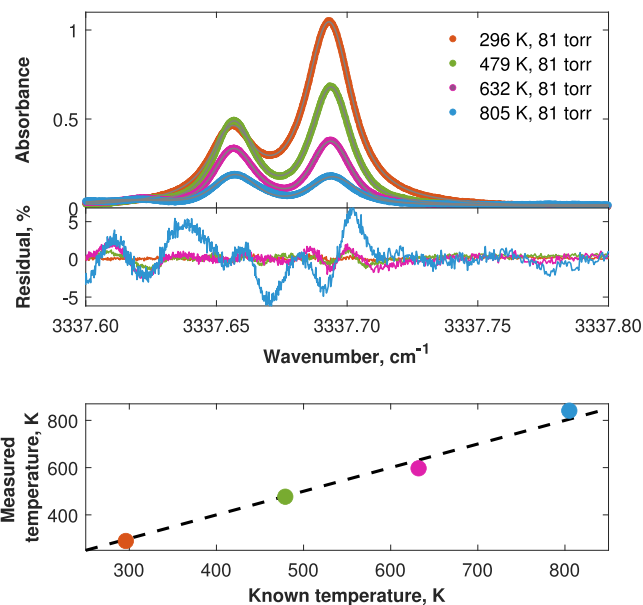


Fig. 5. (Top) Measured  $\text{C}_2\text{H}_2$  spectra at a range of temperatures with spectral fits and accompanying residuals, each normalized by the respective spectrum's peak absorbance value. (Bottom) Measured temperatures obtained from the two-line thermometry technique.

$X_{\text{C}_2\text{H}_4}$  [33]. Prior to performing a least squares fit of the  $\text{CH}_4$  absorbance spectrum, the R(9,14)  $\text{C}_2\text{H}_4$  transition that is in close proximity to the R(3,15) manifold of  $\text{CH}_4$  was omitted from the spectral region of interest. The isolated  $\text{CH}_4$  transition was then fitted using  $X_{\text{CH}_4}$  and  $\phi$  as free parameters.  $\phi$  is defined as a scale factor to the air-broadening coefficient,  $\gamma_{\text{abs,air}}$ , in the collisional linewidth of the transition given by:

$$\Delta\nu_c = 2P_{\text{tot}} [X_{\text{abs}}\gamma_{\text{abs,self}}(T) + \phi(1 - X_{\text{abs}})\gamma_{\text{abs,air}}(T)] \quad (6)$$

Here,  $P_{\text{tot}}$  is the total pressure of the gas mixture and  $\gamma_{\text{abs,self}}$  is the temperature-dependent self-broadening coefficient.  $\gamma_{\text{abs,air}}$  is scaled in this manner in the fitting procedure to account for the absence of broadening coefficient data of the colliding partners in the gas mixture.

To fit the  $\text{C}_2\text{H}_4$  absorbance spectrum, only  $\text{CH}_4$  transitions in the measurement were first fitted as described above. The fitted  $\text{CH}_4$  spectrum was then subtracted from the measurement to yield a residual spectrum that consisted only of the contributions from  $\text{C}_2\text{H}_4$  as shown in the middle subplot of Fig. 6. This residual spectrum was then least-squares fitted with a Voigt profile with  $X_{\text{C}_2\text{H}_4}$  and  $\phi$  treated as free parameters.

To reconcile the optically thick R(15)  $\text{CH}_4$  manifold at elevated temperatures ( $T > 500$  K), a separate region of the spectral scan was used to perform a broadband spectral fit ( $3167.2 \text{ cm}^{-1}$ – $3167.9 \text{ cm}^{-1}$ ) of multiple methane transitions. In this spectral region, interference

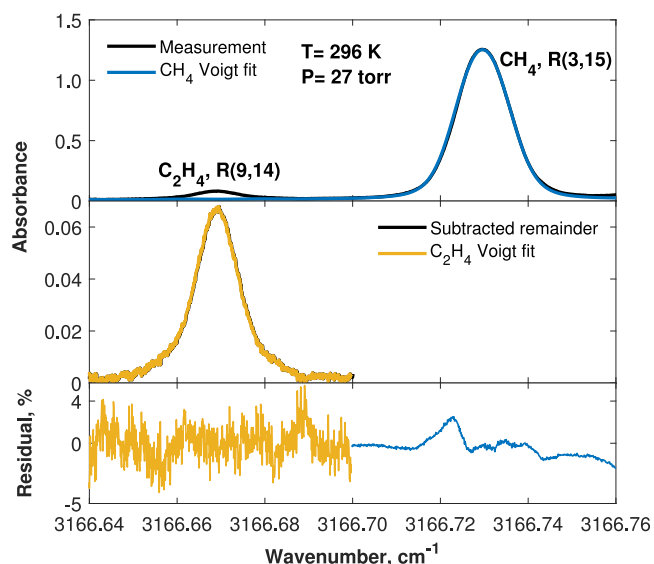


Fig. 6. (Top) Measurement containing both  $\text{CH}_4$  and  $\text{C}_2\text{H}_4$  transitions with a  $\text{CH}_4$  Voigt fit of the spectral region. (Middle) Leftover spectra obtained upon subtraction of the  $\text{CH}_4$  Voigt fit from the measurement. (Bottom) The residuals of the Voigt fits of both species' transitions, normalized by their respective peak absorbance values.

from the other three hydrocarbons in the gas mixture was negligible in magnitude. As before, the free parameters for this least-squares fit were  $X_{\text{CH}_4}$  and  $\phi$ .

### 3.1.3. $\text{CH}_4$ interference mitigation for $\text{C}_2\text{H}_6$ sensing

Accurate determination of  $X_{\text{C}_2\text{H}_6}$  required implementation of a correction method to account for the contribution of broadband  $\text{CH}_4$  interference in the vicinity of the target  $\text{C}_2\text{H}_6$  transitions. Initially, a sequential approach, similar to that used for the determination of  $X_{\text{C}_2\text{H}_4}$ , was employed. The broadband contribution of  $\text{CH}_4$  was removed by subtracting a simulated spectrum from the measurement. This simulation was performed using results ( $X_{\text{CH}_4}$  and  $\phi$ ) obtained from the least squares fit of the measured  $\text{CH}_4$  spectrum near the  $3166\text{ cm}^{-1}$  region and spectral parameters from HITEMP. The spectrum obtained after this subtraction was then least squares fitted similarly with  $X_{\text{C}_2\text{H}_6}$  and  $\phi$  as free parameters. However, this method produced erroneous results, with disagreements of up to 25% in inferred  $X_{\text{C}_2\text{H}_6}$  at elevated temperatures.

Further investigation revealed that spectral simulations using the HITEMP database for  $\text{CH}_4$  exhibited considerable disagreement between the measured peak absorbance of select features and the simulation. This discrepancy is highlighted in Fig. 7, where measurements of pure  $\text{CH}_4$  were made at 3 different temperatures and compared to HITEMP simulations.

Notably, the discrepancy in absorbance between the methane measurement and the HITEMP simulation in the region near the line cluster of  $\text{C}_2\text{H}_6$  ( $\sim 2996.85\text{ cm}^{-1}$ ) is significant (as high as 10% at  $T = 632\text{ K}$ ). Therefore, in this spectral region, a spectral simulation using the HITEMP database proved inadequate to remove the broadband  $\text{CH}_4$  interference. To accurately capture the broadband  $\text{CH}_4$  contribution at this wavelength, absorption cross-sections of pure  $\text{CH}_4$  spectra at  $2996.7\text{ cm}^{-1}$ – $2997.5\text{ cm}^{-1}$  were measured for a range of relevant temperatures and pressures and used to correct the spectral absorption of the multi-species mixtures. The methane cross-section database is included in the supplementary material of this work.

Prior to subtraction from the convoluted measurement, the pure  $\text{CH}_4$  spectrum from the database was scaled by the measured mole fraction of  $\text{CH}_4$  in the test gas. An example of this scaled spectrum overlaid on the convoluted measurement prior to subtraction is shown in the

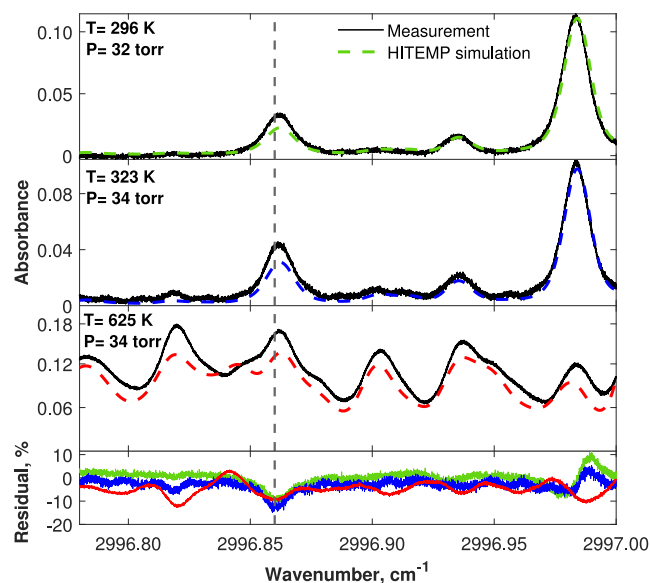


Fig. 7. (Top) Measured pure  $\text{CH}_4$  spectra and HITEMP simulations across a range of temperatures. Dashed lines indicate the linecenter of the target  $\text{C}_2\text{H}_6$  transition. (Bottom) Residuals of the measurement and simulation, normalized by the peak absorbance value of each measured spectrum.

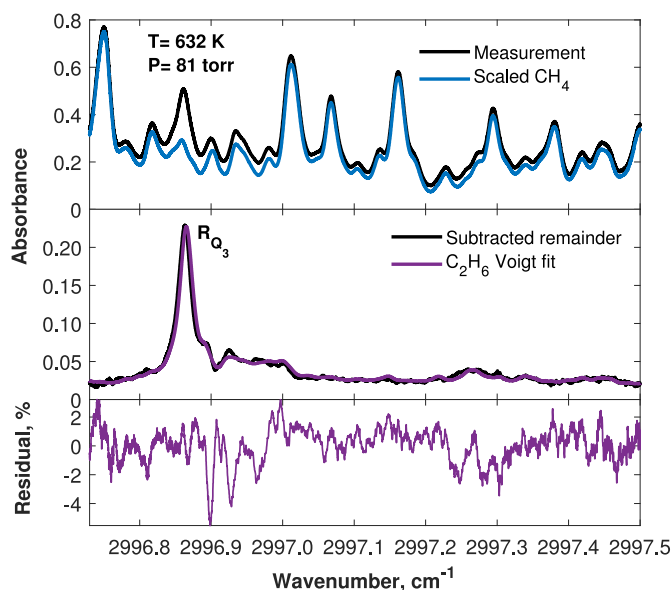


Fig. 8. (Top) Convoluted measurement containing  $\text{C}_2\text{H}_6$  and  $\text{CH}_4$  contributions overlaid with a scaled pure  $\text{CH}_4$  spectrum. (Middle) Leftover spectrum obtained upon subtraction of the scaled pure  $\text{CH}_4$  spectrum from the measurement. (Bottom) Residual of the Voigt fit of the  $\text{C}_2\text{H}_6$  spectrum, normalized by the peak absorbance value of the transitions.

first subplot of Fig. 8. A least squares fit of this remainder spectrum yielded accurate results of  $X_{\text{C}_2\text{H}_6}$  across a range of temperatures and pressures, with measured mole fraction deviation within 5%.

### 3.2. Sensor operating range

As mentioned previously, a gas mixture consisting of the four target hydrocarbon species was used to validate the thermodynamic range and establish detectability limits of the sensor. Fig. 9 shows spectra of all four hydrocarbon species over a representative range of thermodynamic conditions. Room temperature spectra of the species on the top

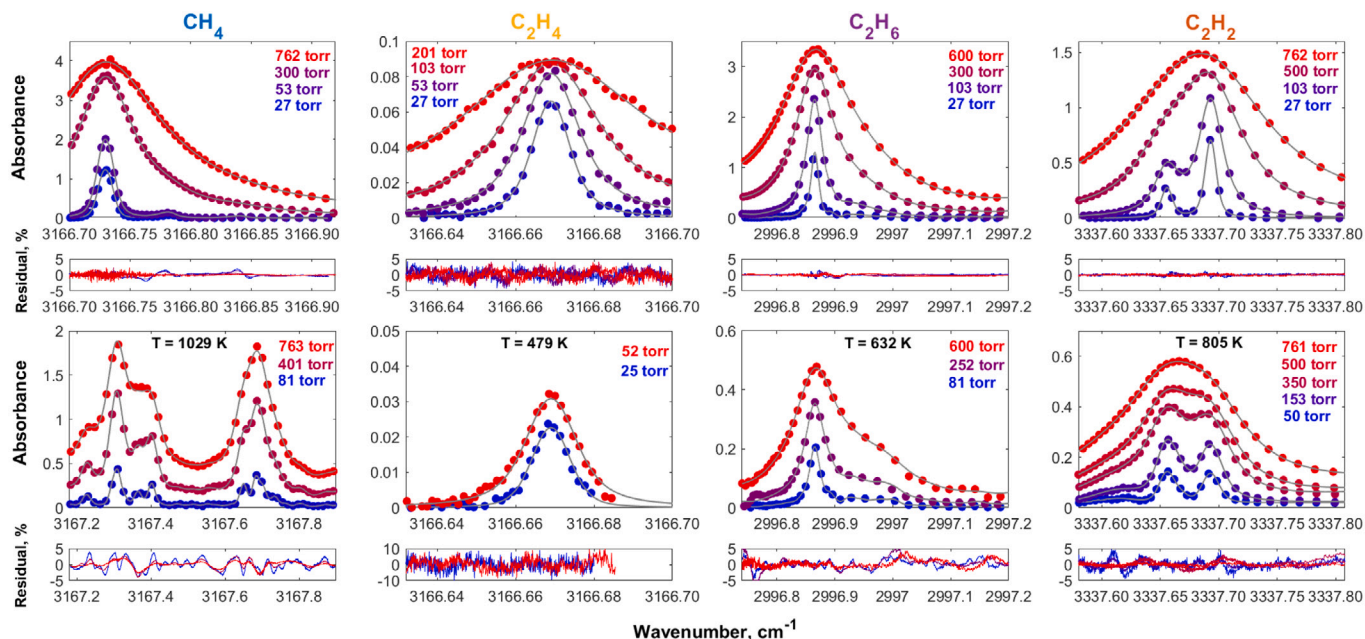


Fig. 9. (L-R) Measured spectra with Voigt fits and accompanying residuals of  $\text{CH}_4$ ,  $\text{C}_2\text{H}_4$ ,  $\text{C}_2\text{H}_6$ , and  $\text{C}_2\text{H}_2$  at  $T = 296$  K (top) and elevated temperatures (bottom) across a range of pressures. Note that the spectral range for  $\text{CH}_4$  is different at 296 K and 1029 K.

row of this figure are combined with respective high-temperature spectra on the bottom. A requisite validation accuracy of 5% in the species mole fraction measurements was imposed to estimate the range of the sensor with respect to temperature and pressure for each species. This threshold was increased to 8% for  $\text{C}_2\text{H}_4$  due to its much weaker absorption feature compared to the other hydrocarbons of interest. For  $\text{CH}_4$ , the spectra were validated up to a maximum temperature of 1029 K through a combination of the two different measurement wavelengths, both shown in Fig. 9. The upper limit of the  $\text{C}_2\text{H}_4$  measurements ( $P = 201$  torr at  $T = 296$  K and  $P = 52$  torr at  $T = 479$  K) was constrained by: (1) the blending of the weaker  $\text{C}_2\text{H}_4$  transition with the much stronger  $\text{CH}_4$  transition at higher pressures and, (2) the progression of the  $\text{C}_2\text{H}_4$  transition into the optically thin regime at higher temperatures. As such, its utility is somewhat constrained to low-pressure applications (including the target solar reactor in this work). The  $\text{C}_2\text{H}_6$  spectra were deconvolved and validated successfully up to approximately 630 K. At higher temperatures, deconvolution of the spectra proved to be more challenging due to the compounding effects of weakening  $\text{C}_2\text{H}_6$  transitions and strengthening  $\text{CH}_4$  transitions with increasing temperature. Coupled with the lack of high-energy transitions in the  $\text{C}_2\text{H}_6$  cross-section database by Harrison et al., inference of  $X_{\text{C}_2\text{H}_6}$  yielded errors near 20% at the next temperature increment ( $\sim 800$  K). Finally, the  $\text{C}_2\text{H}_2$  spectra consisting of the two target transitions were validated up to 805 K (50–760 torr). At higher temperatures, the accuracy of the  $X_{\text{C}_2\text{H}_2}$  measurement diminished. Similarly, the line-by-line database of HITRAN failed to accurately capture the  $\text{C}_2\text{H}_2$  spectra at higher temperatures, likely from a lack of high-energy transitions. Expanding this line-by-line database or building a high-temperature cross-section database would extend the operating range of the current sensor as good SNR remained at such conditions, but such efforts were beyond the scope of this work.

#### 4. Sensor demonstration

In this section, the sensor is demonstrated for time-resolved simultaneous measurements of all four hydrocarbon species on a solar-thermal pyrolysis reactor at a range of experimentally-simulated insolation conditions.

##### 4.1. Experimental setup

The concentrated solar-thermal pyrolysis reactor used in this study is illustrated in Fig. 10. The reactor's hardware and method of operation have been extensively outlined in previous work [23,34], and thus only key elements are included in this work for brevity. In this reactor, concentrated light from a variable output 10 kW<sub>e</sub> xenon lamp that mimics the solar spectrum irradiates a thin porous carbon substrate up to temperatures of 1600 K [35]. An IR camera positioned aft of the reaction zone is used to provide a spatially-resolved temperature measurement of the substrate's rear surface. The concentration of light gives rise to a heat-flux distribution closely described by a Lorentzian distribution, where temperature is highest at the center and lowest at the periphery of the substrate [36].  $\text{CH}_4$  gas (99.999%) is flowed into the reactor chamber and through the 3.2-mm thick porous substrate at known flow rates using a mass flow controller (MKS Instruments), initiating decomposition of the inlet gas. The products of this decomposition reaction, consisting mainly of  $\text{H}_2$ ,  $\text{CH}_4$ , and minor hydrocarbons are expelled through an exhaust line with optical access situated at a vertical distance of 0.29 m from the reaction zone. The LAS sensor module is deployed at this measurement location to characterize the product stream that has cooled to near room temperature, as measured by a thermocouple and confirmed by the acetylene sensor at that location.

For the purpose of this demonstration, the start-up transient response of the reactor is studied at a range of lamp output powers. Leveraging the variable power output of the lamp, the intensity of irradiation incident on the substrate is modulated, effectively controlling the temperature of the reaction zone. The power output of the lamp for these experiments ranged from 0.92 to 2.34 kW while the volumetric flow rate of the  $\text{CH}_4$  feed gas and pressure of the reactor are kept constant at 100 sccm and 25 torr, respectively. At each output power condition, the lamp power output is allowed to reach steady state over the course of several minutes. During this period, the substrate is blocked from the lamp's concentrated light by a motorized douser to prevent any fluctuations in the output of the lamp from influencing the decomposition process. Once steady state output of the lamp is established,  $\text{CH}_4$  flow into the reaction zone is initiated and the motorized douser is opened, thus commencing the heating of the substrate and decomposition reaction.

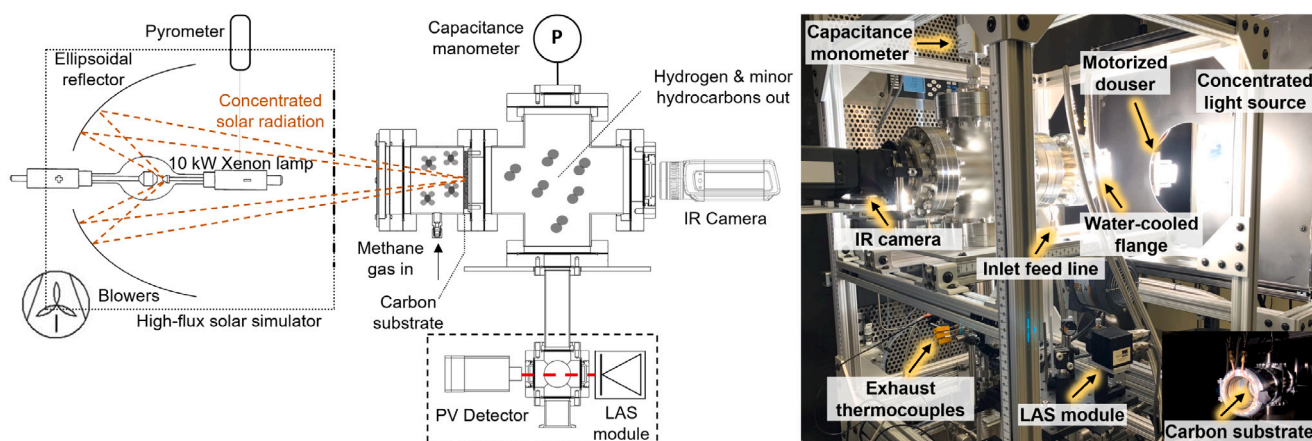


Fig. 10. (Left) Schematic of the solar-thermal pyrolysis reactor with the LAS sensor module located at the exhaust of the reactor. (Right) A photograph of the reactor during operation.

#### 4.2. Results and discussion

The time-division-multiplexed colinear delivery of the three beams at the reactor exhaust facilitated time-resolved simultaneous measurements of all four hydrocarbon species during the decomposition of  $\text{CH}_4$ , as shown in Fig. 11. Knowledge of these four hydrocarbon species mole fractions provides an indirect measurement of the  $\text{H}_2$  mole fraction at any given time by invoking the major products assumption to formulate the equation given below:

$$X_{\text{H}_2} = 1 - (X_{\text{CH}_4} + X_{\text{C}_2\text{H}_6} + X_{\text{C}_2\text{H}_4} + X_{\text{C}_2\text{H}_2}) \quad (7)$$

Implicit in Eq. (7) is that any minor product excluded in the accounting of the gaseous species forms only in negligible quantities. This is corroborated through supporting mass spectrometry measurements on the reactor [23]. While not tested here, it is notable that the major products assumption is also expected to remain valid for applications with natural gas mixtures that consist primarily of  $\text{CH}_4$  and other larger hydrocarbons common to natural gas. During pyrolysis, these larger hydrocarbons (such as ethane, propane, and butane) are expected to similarly decompose into the target C1-C2 intermediates and follow the dehydrogenation pathway of  $\text{CH}_4$  as in Eq. (2). However, application of this method with feedstocks that contain appreciable quantities of non-hydrocarbon species such as  $\text{CO}_2$  and  $\text{N}_2$  which are also common constituents in natural gas, will require modification of Eq. (7) based on a known initial concentration of these inert species. The inclusion of a  $\text{C}_2\text{H}_2$  measurement, a key product in the decomposition of  $\text{CH}_4$ , significantly improves and simplifies  $\text{H}_2$  yield determination compared to our previous work [23]. Without this measurement, several additional analytical steps such as hydrogen and carbon atom balancing must be first implemented to determine  $X_{\text{C}_2\text{H}_2}$  before application of Eq. (7) is possible [23]. To account for the carbon atoms in particular, physical measurement of the mass of deposited carbon on the substrate surface at the end of each experiment was required, which prevented a time-resolved measurement of hydrogen yield, as is demonstrated here. As such, the present work enables the direct application of Eq. (7) at every measurement interval throughout the duration of the experiment and, importantly, provides a transient quantification of the  $X_{\text{H}_2}$  yield. The evolution of  $X_{\text{H}_2}$  is shown in Fig. 11.

Across all species measurements, an apparent lag is observed between the time at which the motorized douser is opened and the detection of the initiation of the decomposition process. This time lag can be attributed to: (1) the transit time of the product gas from the reaction zone to the LAS measurement location and (2) the thermal ramp up of the reaction zone from room temperature due to the irradiation of the concentrated light on the substrate surface. The transit time of the product gas contributes to approximately 3 s of this observed latency

as demonstrated in calculations provided in Appendix A. Based on the mass (~4 g), heat capacity, and absorptivity of the carbon substrate, a thermal ramp up period on the order of seconds is expected from direct irradiation. This contrasts volumetric reactors with indirect heating which can require up to hours to achieve steady-state conditions [37]. The rapid heating timescales of this reactor are observed in the experimental data, through both the thermal imaging of the substrate's rear surface and the accompanying time-resolved speciation of the products shown in Fig. 11. The time at which decomposition initiates across all lamp output power conditions shows a strong correlation with this ramp up period, with decomposition beginning only after the substrate surface temperature passes ~1000 K, reflective of the highly temperature-dependent reaction kinetics.

The rate of  $\text{CH}_4$  decomposition demonstrates a strong correlation with lamp output power which directly influences substrate temperature. To quantify this effect, the time taken for  $X_{\text{CH}_4}$  to reach 1/e (~63%) of its equilibrium change in magnitude from the point at which the concentrated light was introduced in the chamber was studied across all lamp output powers. At the extrema of the lamp's output power, this time was measured to be approximately 50 s at 0.92 kW and 10 s at 2.34 kW, accounting for the transit time of the gas from the reaction zone. As expected, the higher reaction zone temperatures associated with higher lamp output powers facilitate more rapid decomposition of the inlet  $\text{CH}_4$  stream, resulting in a five-fold increase in decomposition rate at the extremes. This effect may be attributed to the exponential Arrhenius-like temperature dependence in the chemical timescale associated with the cracking of the  $\text{CH}_4$  molecules at higher temperatures [38].

The strong dependence of this process on temperature (or lamp output power) is also captured in the steady-state compositions of the product stream across multiple experiments. An increase in the output power from 0.92 kW to 2.34 kW, corresponding to an increase in steady-state peak temperature of approximately 250 K on the substrate surface, substantially altered the composition of the product stream. Across this output power range, the steady-state  $\text{CH}_4$  composition for example, fell from 58% to 11%, representing a significant increase in methane conversion. Analogous trends are observed across the other measured hydrocarbons, excluding  $\text{C}_2\text{H}_2$ . The steady-state  $\text{C}_2\text{H}_2$  composition in the product stream is minimally affected by changes in output power of the lamp, with mole fractions only varying within 15% of the measured maximum.

The steady-state composition of the product stream further indicates an incomplete decomposition process. For example, decomposition at the highest lamp output power resulted in a measured steady-state product composition of approximately 85%  $\text{H}_2$ , 11%  $\text{CH}_4$ , 2.9%  $\text{C}_2\text{H}_2$ , 0.7%  $\text{C}_2\text{H}_4$ , and 0.05%  $\text{C}_2\text{H}_6$ . Incomplete decomposition of the  $\text{CH}_4$



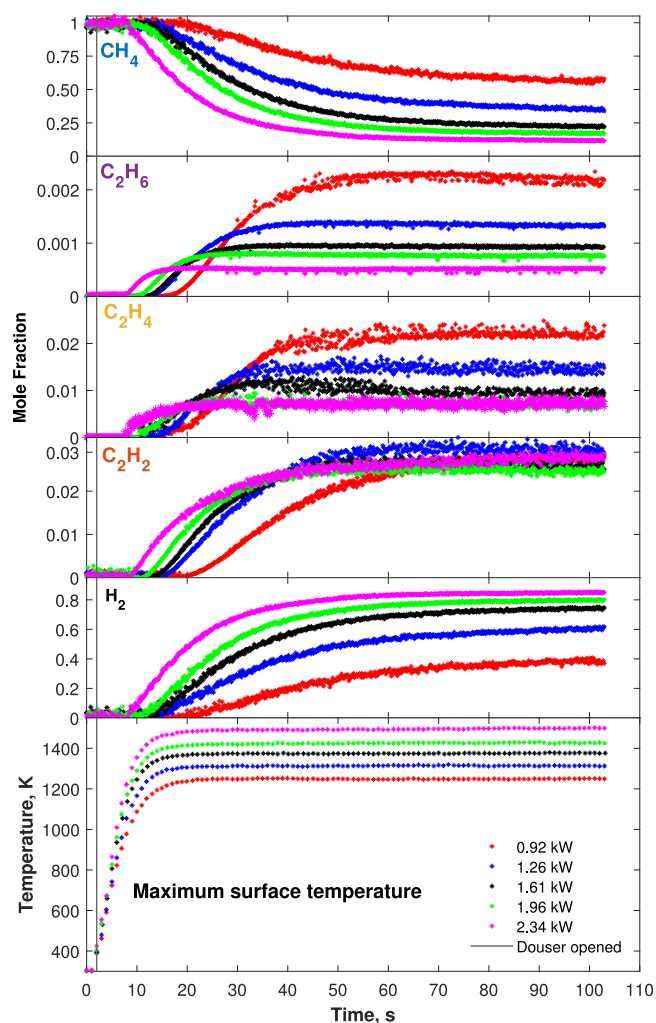


Fig. 11. (Top) Transient mole fraction measurements of  $\text{CH}_4$ ,  $\text{C}_2\text{H}_6$ ,  $\text{C}_2\text{H}_4$ , and  $\text{C}_2\text{H}_2$  and calculated mole fractions of  $\text{H}_2$  across a range of lamp output powers. (Bottom) Maximum rear surface temperature of the carbon substrate.

feed gas is partially attributed to the non-uniform temperature distribution of the reaction zone. This non-uniform temperature distribution, with large variations in temperature between the hot and cold regions of the porous substrate gives rise to a spatially-inhomogeneous decomposition reaction. Regions at higher temperatures facilitate greater progression of the decomposition along the dehydrogenation pathway. In contrast, colder regions inhibit complete decomposition of  $\text{CH}_4$ , with these temperatures yielding greater quantities of the lower C:H intermediate species. Regions on the periphery of the substrate with surface temperatures around 700 K likely prevent any decomposition of  $\text{CH}_4$  at all, allowing the inlet  $\text{CH}_4$  gas to flow through unreacted. It should be noted that the magnitudes of the minor hydrocarbons are generally higher than that predicted by chemical equilibrium, suggesting that the reacting flow is getting kinetically frozen along the reaction path where higher mole fractions are observed (see Fig. 1).

The measured species evolutions at the start-up of the reactor are similarly consistent with the dehydrogenation kinetic pathway defined in Eq. (2). This stepwise dehydrogenation of  $\text{CH}_4$  is captured in the relative durations taken by the minor species to reach steady-state. The measurements show the first minor hydrocarbon in the reaction pathway,  $\text{C}_2\text{H}_6$ , reaches steady-state the earliest followed by  $\text{C}_2\text{H}_4$  and finally  $\text{C}_2\text{H}_2$ , in increasing order of C:H ratio. The time taken to reach steady-state for  $\text{C}_2\text{H}_6$  and  $\text{C}_2\text{H}_4$  are similar, likely due to  $\text{C}_2\text{H}_6$  being

relatively unstable at these reaction temperatures and decomposing quickly to form  $\text{C}_2\text{H}_4$ . This behavior is more pronounced at the lower power input (such as the 0.92 kW case) reflective of the slower kinetics and longer timescales generally. The trends are also corroborated through kinetic simulations of  $\text{CH}_4$  decomposition in CANTERA, as shown in Fig. 1.

The measurement precision (or  $1\sigma$  detection limit) of the sensor in the solar reactor environment is estimated by calculating the minimum resolvable absorbance for each species which occurred during the transient measurements. The measurement resolution is estimated to be 0.2% for  $\text{CH}_4$ , 700 ppm for  $\text{C}_2\text{H}_2$ , 600 ppm for  $\text{C}_2\text{H}_4$ , and 30 ppm for  $\text{C}_2\text{H}_6$  at an optical pathlength of 8.2 cm, pressure of 25 torr, and temperature of 298 K. The relative uncertainty for all species lies in the 3%–13% range primarily due to uncertainties in the spectroscopic reference parameters and the conditions of the reactor. These uncertainties are limited by noise/precision limits at the early formation times for acetylene, ethylene, and ethane but for most of the test duration and always for methane, the SNR was greater than 10. The measurement resolution of  $\text{H}_2$  is inferred to be approximately 0.3%, and the estimated uncertainty in inferred  $X_{\text{H}_2}$  is ~4%, obtained by summing the measurement uncertainties of each hydrocarbon in quadrature whilst also accounting for their relative proportions in the product stream at a typical operating condition. Given the indirect quantification of  $\text{H}_2$  yield and the relative abundance of  $\text{CH}_4$  in the product stream, this resolution value is heavily dominated by the resolution and uncertainty of the  $\text{CH}_4$  measurement. Further details on uncertainty calculations may be found in the appendix.

## 5. Conclusion

In this work, a mid-infrared laser absorption sensor was developed for simultaneous time-resolved species measurements of the four most abundant hydrocarbons ( $\text{CH}_4$ ,  $\text{C}_2\text{H}_2$ ,  $\text{C}_2\text{H}_4$ , and  $\text{C}_2\text{H}_6$ ) in the pyrolysis of natural gas or methane, providing for a measurement of hydrogen yield through molar balance. The fundamental C-H stretch vibrational bands in the 3.00–3.34  $\mu\text{m}$  wavelength range were exploited to probe multiple strongly absorbing transitions of these hydrocarbons. A time-division multiplexed technique combined with correction methods to remove cross-species spectral interference was employed to successfully obtain mole fraction measurements of the four species at a repetition rate of 10 kHz.

In addition, two neighboring  $\text{C}_2\text{H}_2$  transitions were leveraged for the application of a two-line thermometry technique that yielded accurate inference of gas temperature up to 805 K. The thermodynamic range of the sensor was further validated across a range of temperatures and pressures on a high-temperature gas cell using mixture compositions relevant to the decomposition of natural gas and methane at sub-atmospheric pressures. While acetylene and methane exhibited good detectability up to 800–1000 K, ethylene and ethane detectability was limited to lower temperatures (~600 K), with limitations associated with the inverse temperature dependence of differential absorbance, spectral database inadequacies, and convolution by spectral interference from methane. A database of methane cross-sections in the 2996.7  $\text{cm}^{-1}$ –2997.5  $\text{cm}^{-1}$  range was built for interference mitigation of the ethane measurement and is included in the supplementary material up to a temperature of 805 K.

The multi-species sensing capability was demonstrated for in situ analysis in a solar-thermal pyrolysis reactor, where simultaneous time-resolved species measurements elucidated the transient behavior of the reactor at a range of experimentally-simulated insolation conditions. The sub-atmospheric operating envelope of the reactor provided for high-quality measurements of all 4 target species and time-resolved quantification of  $X_{\text{H}_2}$  through the major products assumption. These measurements demonstrated the utility of the sensor for deployment in hydrocarbon pyrolysis reactors and solar-thermochemical systems, where real-time monitoring of the product stream is critical for robust

process control due to intermittency of insolation throughout a given day. Future work is expected to leverage the expanded operating range of this sensor to perform species measurements further upstream in the solar pyrolysis reactor, near the heterogeneous reaction zone, to further understand the chemical physics involved.

### Declaration of competing interest

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests: TSF and RMS are co-founders of a company (SolGraph Inc.) that is involved with solar-thermal material synthesis. The submitted work is an academic study outside the scope of this activity and is not intended or represented as a commercial product or promotion.

### Data availability

The methane cross-sections are available as supplementary material to the article. Other data are available upon request.

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### Appendix A. Product gas transit time

The transit time of the product gas from the heterogeneous reaction zone to the LAS measurement location was calculated using the equation below:

$$\tau = \frac{L\rho A}{\dot{m}} \quad (\text{A.1})$$

Here,  $L$  is the total distance traveled by the gas,  $\rho$  is the density of the gas (assumed to be pure  $\text{CH}_4$  at the start of decomposition),  $A$  is the cross-sectional area of the flow, and  $\dot{m}$  is the mass flow rate of the gas. In the evaluation of the transit time, the non-uniform cross-sectional areas of the reaction chamber and the exhaust tube were considered separately when evaluating Eq. (A.1). The individual results were then summed to obtain a final representative value. Given the transient nature of the process, an aggregate gas temperature of 800 K was assumed in the reaction chamber and 300 K in the exhaust tube to approximate  $\rho$ .

### Appendix B. Uncertainty analysis

The Taylor series method (TSM) of uncertainty propagation [23] was applied with reference to Eq. (4) to calculate the relative uncertainties in the measured mole fractions as follows:

$$\frac{\Delta X_{\text{abs}}}{X_{\text{abs}}} = \sqrt{\left(\frac{\Delta \alpha_v}{\alpha_v}\right)^2 + \left(\frac{\Delta P}{P}\right)^2 + \left(\frac{\Delta S_i(T)}{S_i(T)}\right)^2} \quad (\text{B.1})$$

Here, a 0.5% uncertainty is used for the pressure measurement and linestrength uncertainties are obtained from the respective spectroscopic databases. The uncertainty in temperature at the measurement conditions of the reactor (near room temperature) is minor and is thus excluded from Eq. (B.1). Applying Eq. (B.1) at a representative condition during the decomposition of  $\text{CH}_4$  at the highest lamp output power (2.34 kW) yielded species uncertainties of 2.5% in  $\text{CH}_4$ , 4% in  $\text{C}_2\text{H}_2$ , 11% in  $\text{C}_2\text{H}_4$ , and 3% in  $\text{C}_2\text{H}_6$ , respectively.

$$\Delta X_{\text{H}_2} = \sqrt{\left(\frac{\partial X_{\text{H}_2}}{\partial X_{\text{CH}_4}} \Delta X_{\text{CH}_4}\right)^2 + \left(\frac{\partial X_{\text{H}_2}}{\partial X_{\text{C}_2\text{H}_2}} \Delta X_{\text{C}_2\text{H}_2}\right)^2 + \left(\frac{\partial X_{\text{H}_2}}{\partial X_{\text{C}_2\text{H}_4}} \Delta X_{\text{C}_2\text{H}_4}\right)^2 + \left(\frac{\partial X_{\text{H}_2}}{\partial X_{\text{C}_2\text{H}_6}} \Delta X_{\text{C}_2\text{H}_6}\right)^2} \quad (\text{B.2})$$

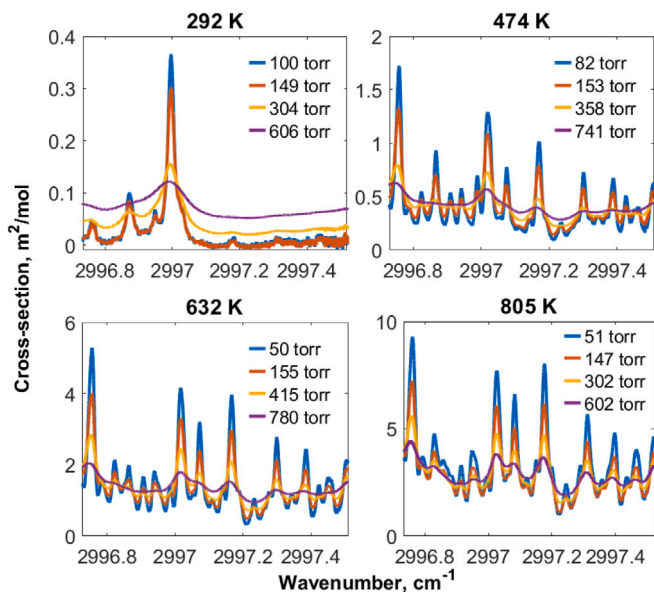


Fig. C.12. Select  $\text{CH}_4$  cross-sections across a range of temperatures and pressures. The cross-sections given at each temperature and pressure represent an average of the cross-sections collected for a single test.

### Appendix C. Supplementary data

The supplementary material consists of four absorption cross-section files:  $\text{CH}_4\_cross\_sec\_292\text{K}.csv$ ,  $\text{CH}_4\_cross\_sec\_474\text{K}.csv$ ,  $\text{CH}_4\_cross\_sec\_632\text{K}.csv$ , and  $\text{CH}_4\_cross\_sec\_805\text{K}.csv$  are comma-separated values files of the measured  $\text{CH}_4$  cross-sections in the  $2996.7\text{ cm}^{-1}$ – $2997.5\text{ cm}^{-1}$  range at 292 K, 474 K, 632 K, and 805 K respectively. The pressures are varied from 50 to 780 torr to include spectra dominated by Doppler and pressure broadening. All the measurements are performed in pure  $\text{CH}_4$ . The first row of these files contains the pressures at which each cross-section measurement was made, in *torr*. The second row and first column constitute the wavenumber and each subsequent column is the cross-section at each pressure, in  $\text{mol}/\text{m}^2$ . These cross-sections are represented in Fig. C.12.

Supplementary material related to this article can be found online at <https://doi.org/10.1016/j.jaecs.2023.100223>.

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